

Ecole de Métallurgie Fondamentale

Action Nationale de Formation (ANF)

22-25 Octobre 2012, Aussois

Métaux et Alliages sous Irradiation

P. Pareige

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EDF, Les Renardières

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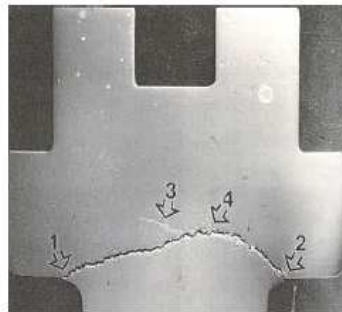
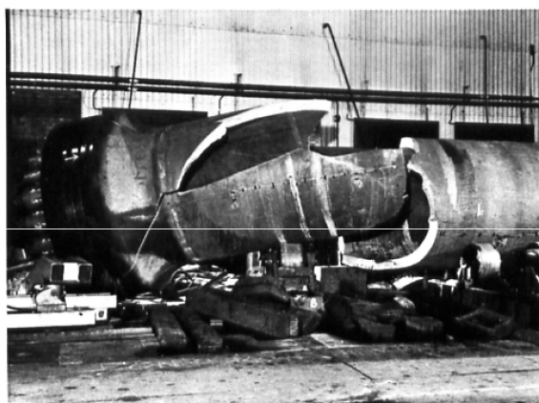
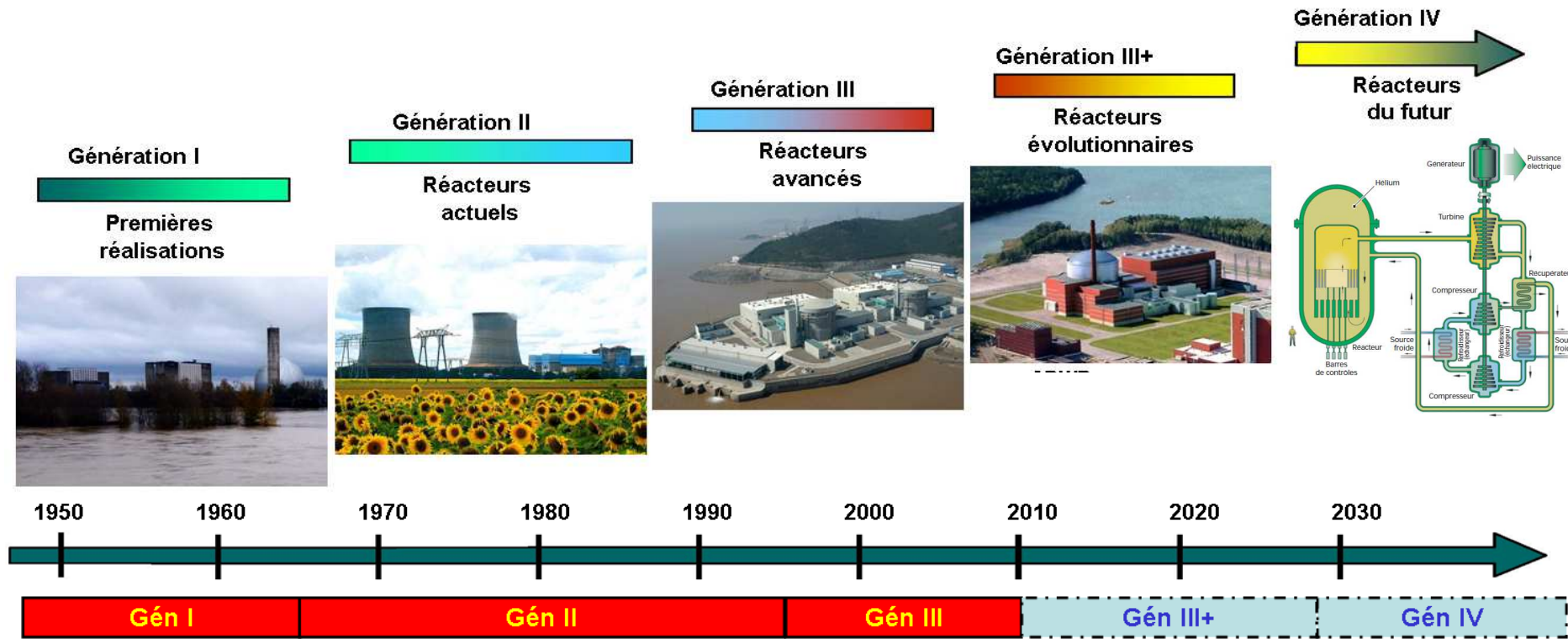
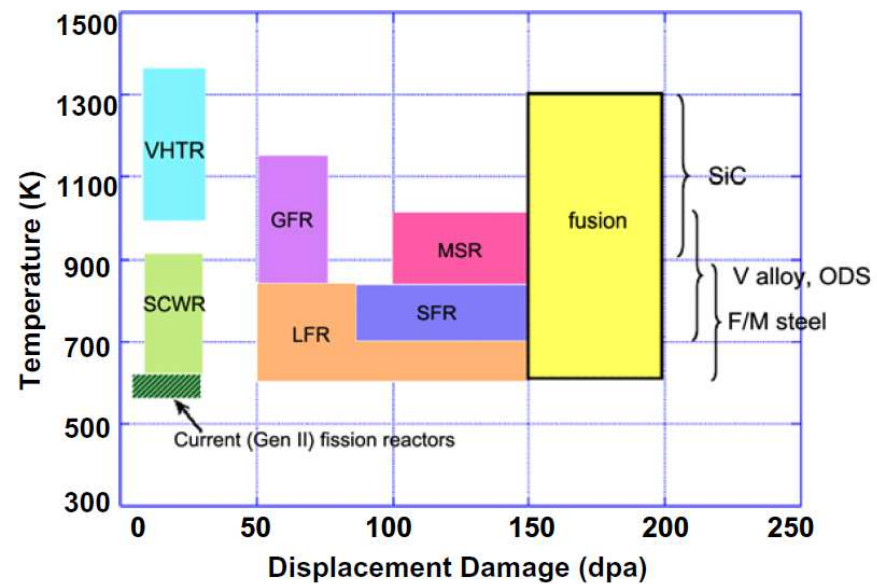


Fig. 1.12. Failure by brittle fracture of thick-walled cylindrical pressure vessel during hydraulic test (By courtesy of John Thompson Ltd., Wolverhampton)



Outline

Interaction ion-matter

Ballistic Damage (primary damage)

- Frenkel pairs
- Atomic Displacement Cascade
- Disorder induced by ballistic damage

Properties of point defects and their clusters :

- Structure
- Mobility

Slow evolution (secondary damage) :

- Evolution of the point defects population:
- Consequence of the super-saturation of point defects
 - Agglomeration of point defects
 - Enhanced phase transformation
 - Induced Segregation and precipitation

Macroscopic Consequences

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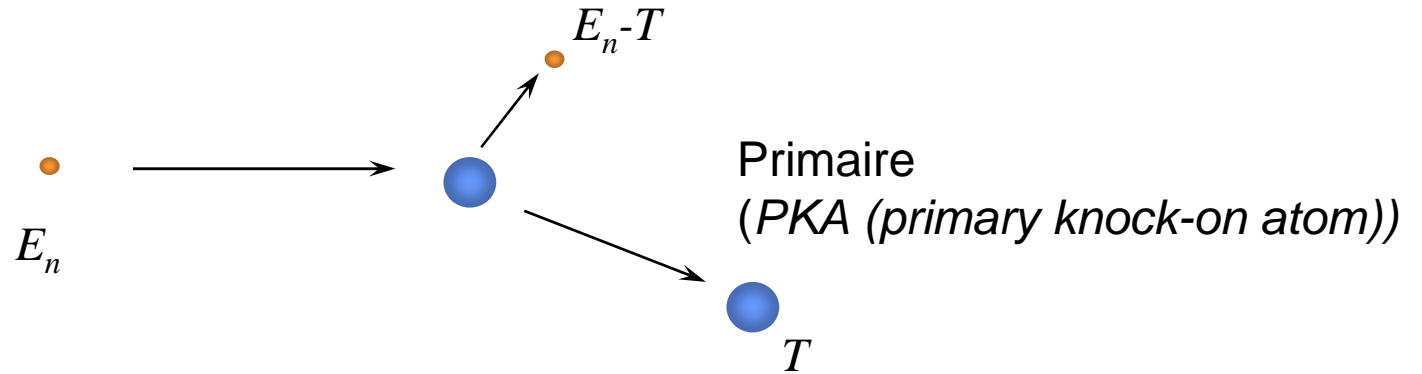
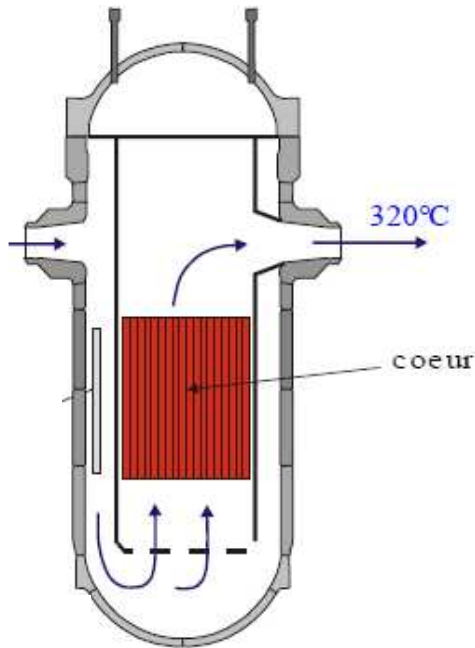
Slow evolution (secondary damage) :

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Macroscopic Consequences

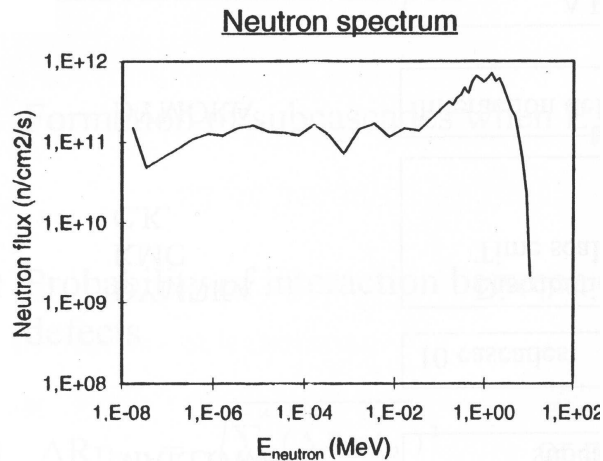
Origine du dommage d'irradiation: collision élastique

Neutron → Chocs élastiques avec les noyaux



$$\bar{T} = \frac{T_{\text{Max}}}{2}$$

$$T_{\text{Max}} = 4 \frac{m_n \cdot m_c}{(m_n + m_c)^2} E_n$$

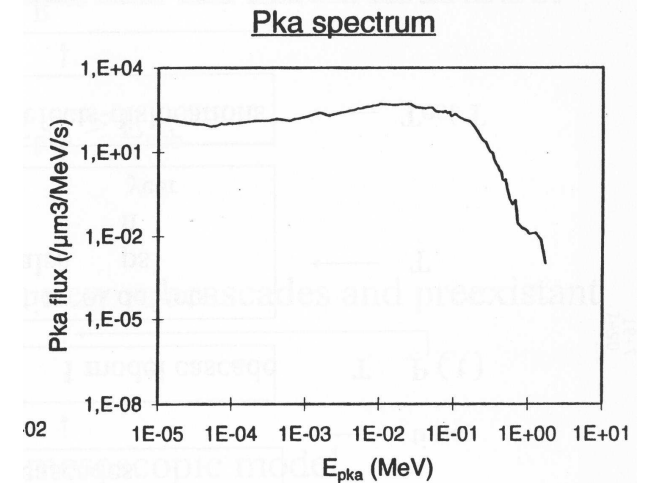


Ex: neutron de 1 MeV

sur un atome de fer

$T_{\text{max}} \sim 70 \text{ keV}$

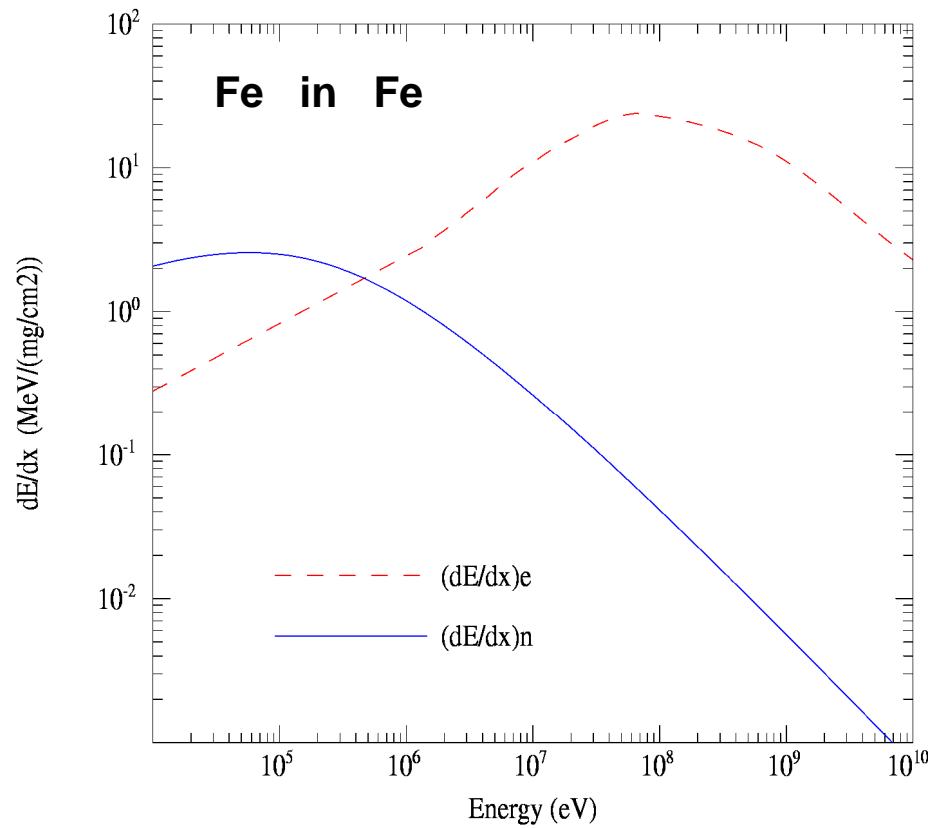
$\langle T \rangle \sim 35 \text{ keV}$



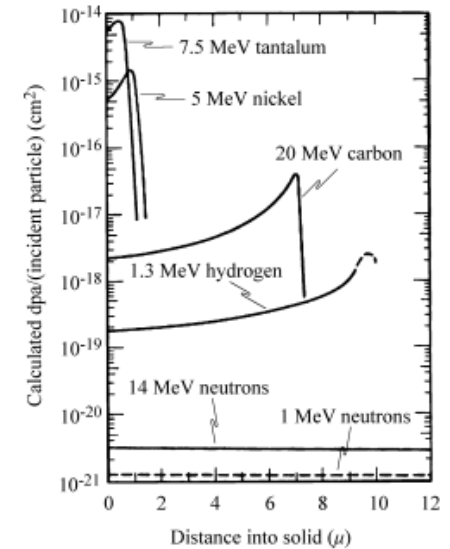
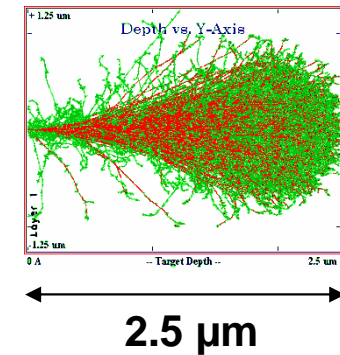
Interaction Ions-Métal

Collisions Elastique et Inélastique

Energy loss per unit path



Stopping and Ranging of Ions in Matter (SRIM)

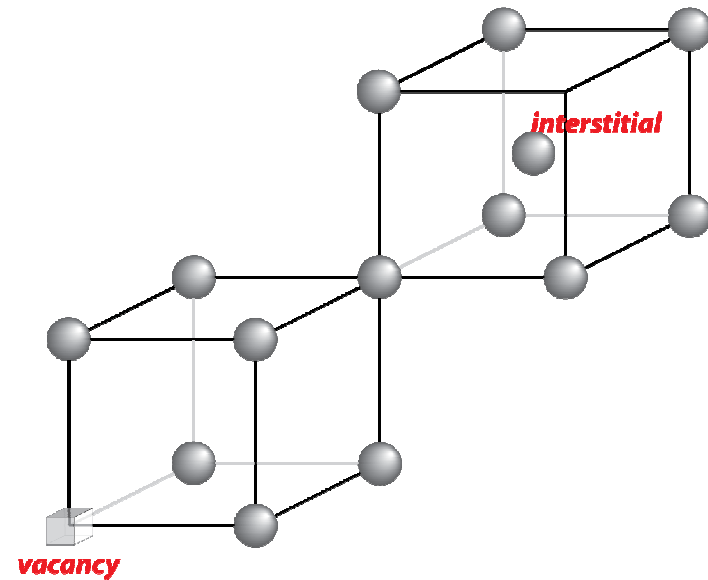
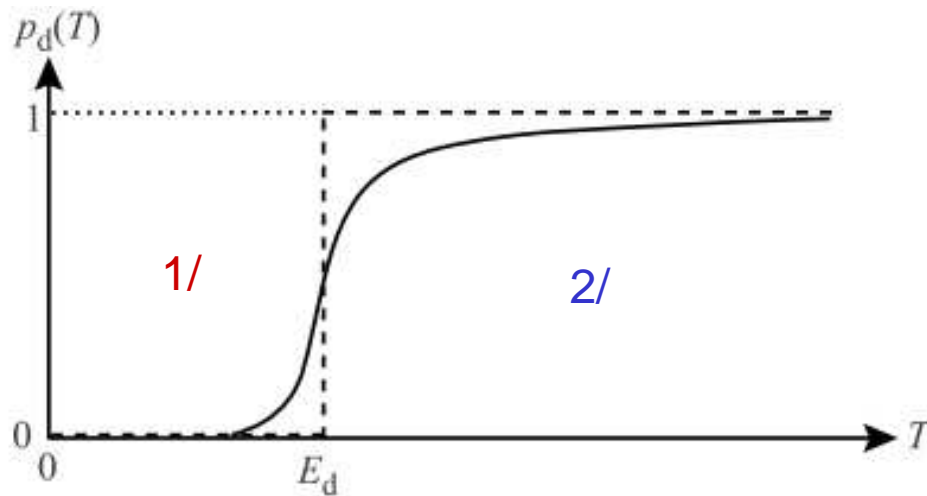


Domage ballistique : seuil de déplacement

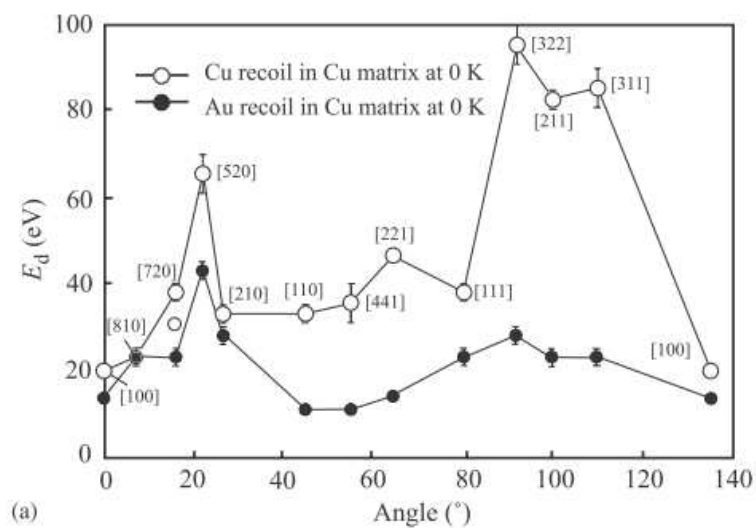
E_d = displacement threshold

1/ $T < E_d$: Phonon – Recombination

2/ $T > E_d$ but is low : single **Frenkel pair**
(one vacancy + one interstitial)



Domage ballistique : seuil de déplacement



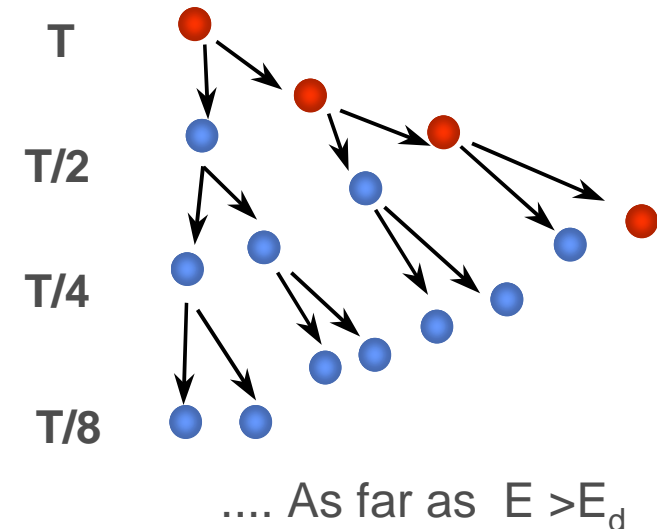
Metal	Lattice (c/a)	$E_{d,min}$ (eV)	E_d (eV)
Al	fcc	16	25
Ti	hcp (1.59)	19	30
V	bcc	–	40
Cr	bcc	28	40
Mn	bcc	–	40
Fe	bcc	20	40
Co	fcc	22	40
Ni	fcc	23	40
Cu	fcc	19	30
Zr	hcp	21	40
Nb	bcc	36	60
Mo	bcc	33	60
Ta	bcc	34	90
W	bcc	40	90
Pb	fcc	14	25
Stainless steel	fcc		40

Domage ballistique : cascade de déplacements

3/ If $T \gg E_d$ Atomic displacement cascade

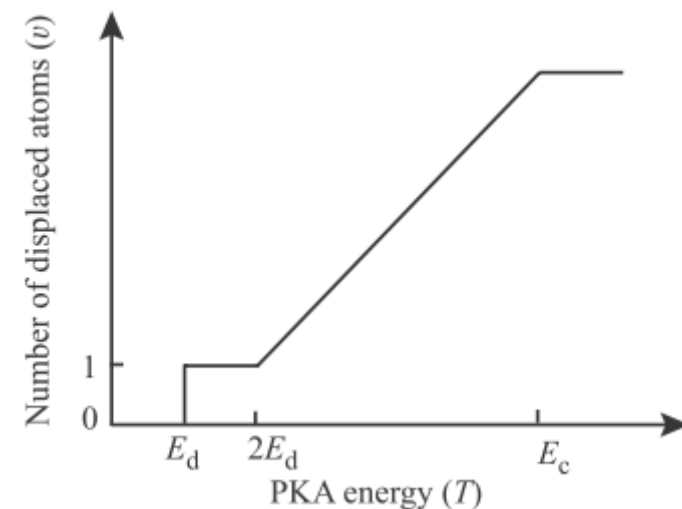
Modèle de Kinchin-Pease

- 1- Cascade = suite de collisions à 2 corps (sphères dures)
- 2- $P_d(T) = 1$ si $T > E_d$ et 0 sinon
- 3- Pas d'énergie transférée au réseau ou sous forme d'excitation électronique
- 4- si $T > E_c$, pas de défauts supplémentaires
- 5- Arrangement aléatoire des atomes



Number of displaced atoms (Frenkel pairs) :

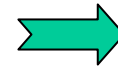
$T < E_d$	$N_d = 0$
$E_d < T < 2 E_d$	$N_d = 1$
$2 E_d < T < E_c$	$N_d = T / (2 \cdot E_d)$
$T > E_c$	$N_d = E_c / (2 \cdot E_d)$



Dommage ballistique : cascade de déplacements

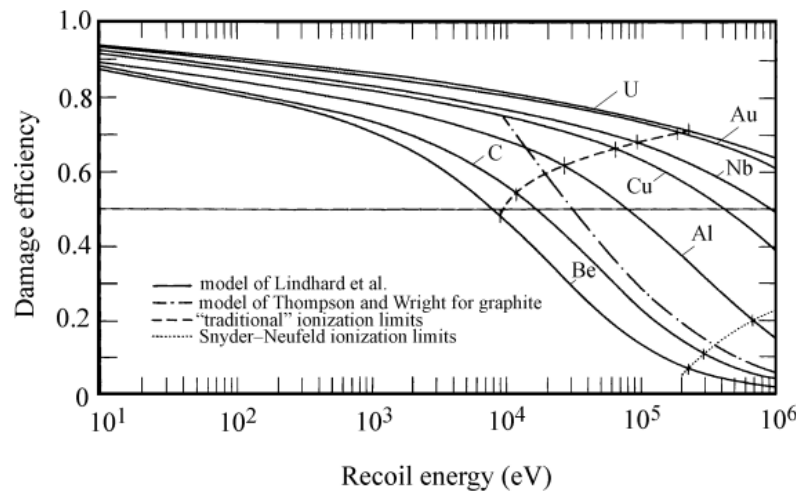
Modèle de Norgett, Robinson, Torrens (NRT)

- Potentiel d'interaction plus réaliste
- Excitation électronique



$$N_d = \frac{\kappa E_D}{2E_d} = \frac{\kappa(T - \eta)}{2E_d}$$

→ Efficacité de déplacement (κ):



→ Energie de dommage (E_D):

T : énergie total du PKA
 η : énergie perdue par excitation électronique dans la cascade

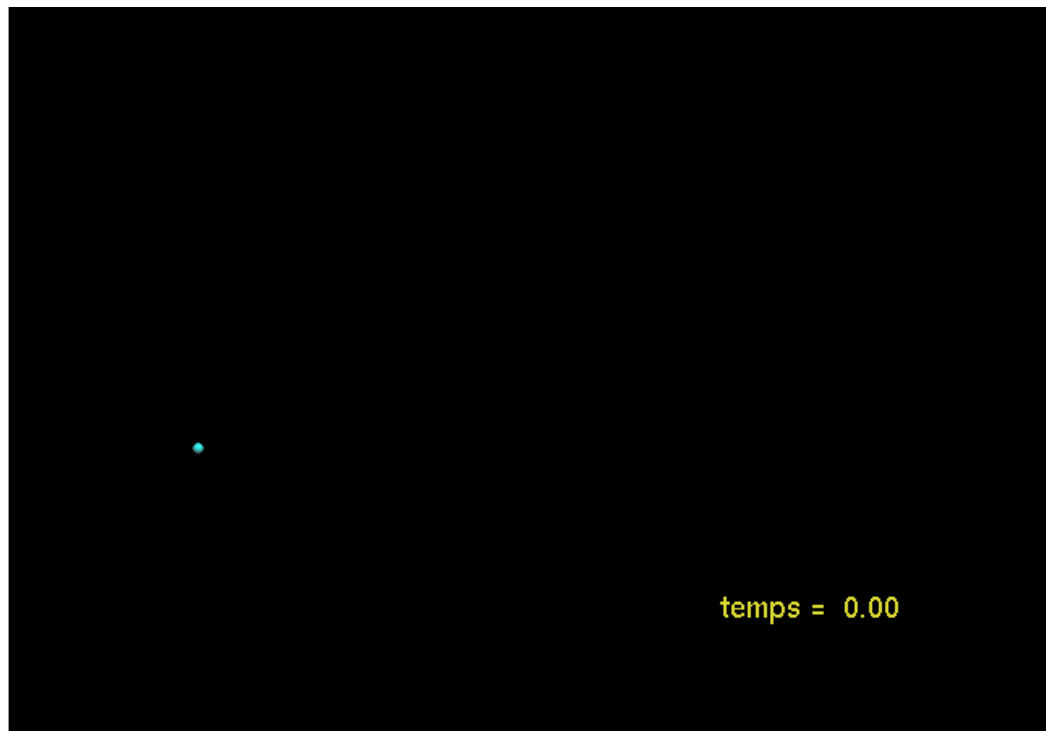
NRT

Number of displaced atoms

$T < E_d$	$N_d = 0$
$E_d < T < 2,5 E_d$	$N_d = 1$
$2,5 E_d < T < E_c$	$N_d = E_D / (2 \cdot E_d)$

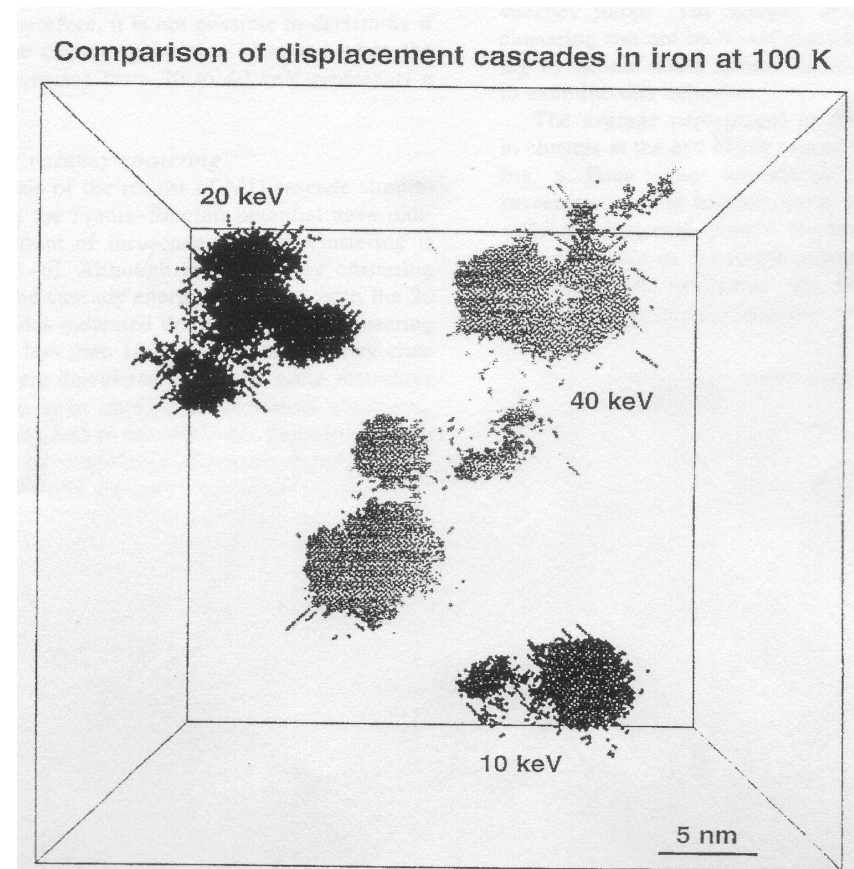
Domage ballistique : cascade de déplacements

Autre moyen d'étudier la cascade de déplacement : la modélisation : dynamique moléculaire



Sim. Dynamique Moléculaire: CEA Saclay

$$\frac{d^2 \vec{r}_i}{dt^2} = m_i^{-1} \left(- \frac{\partial E}{\partial \vec{r}_i} \right)$$

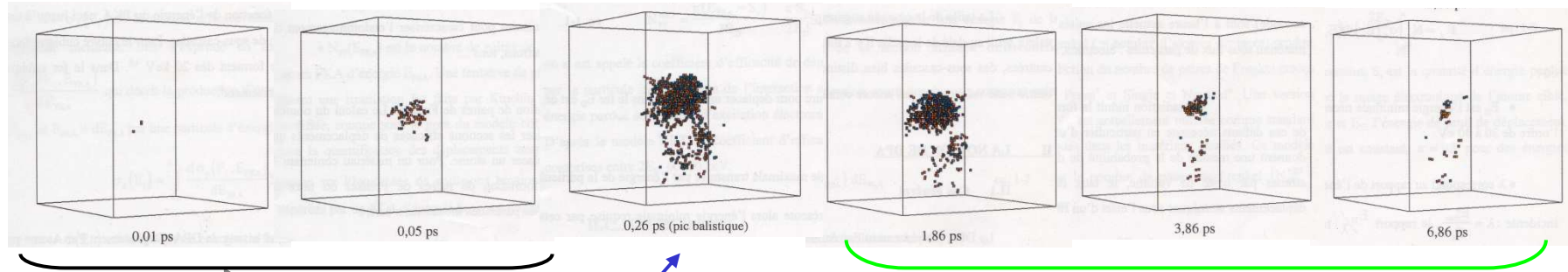


[R. E. Stoller, JNM, 1997]

Formation de sous cascades à haute énergie

Domage ballistique : cascade de déplacements

4 keV Displacement cascade in Iron
Molecular Dynamic Simulation (C. Domain - EDF)



Collisions

Nombre de défauts
ponctuels

Pic
ballistique

Recombinaison

DP résiduels
(libres et amas)

Temps

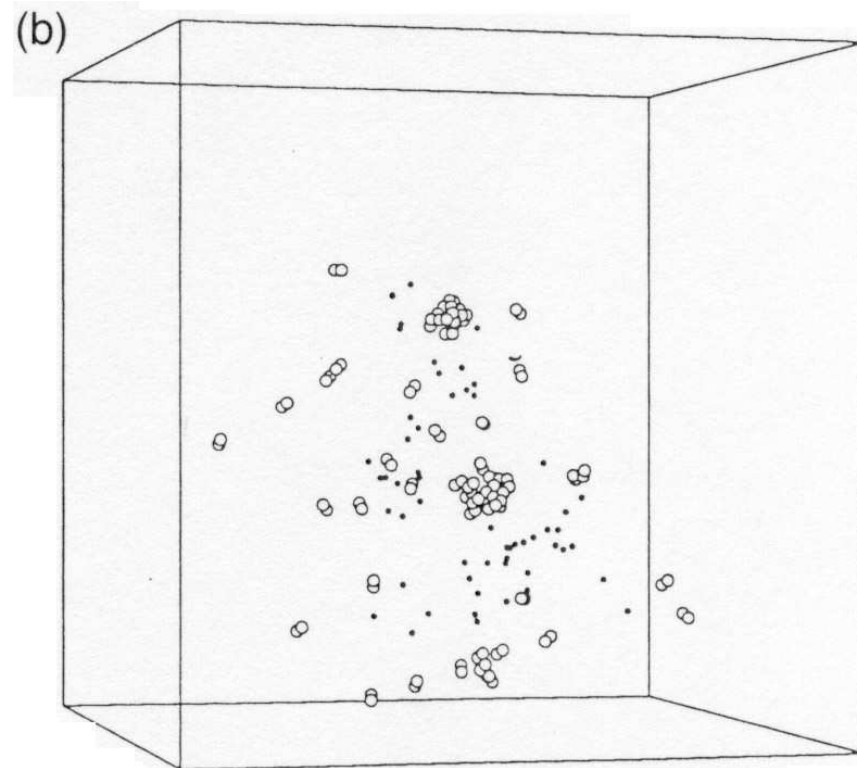
1 ps

10 ps

Qu'est ce qu'un résidu de cascade....?

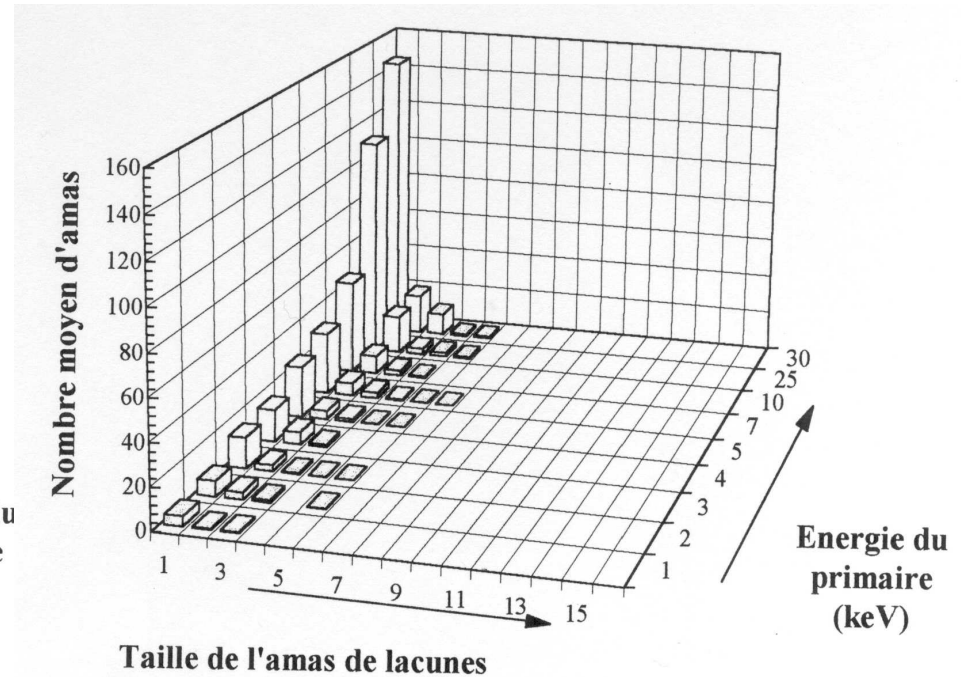
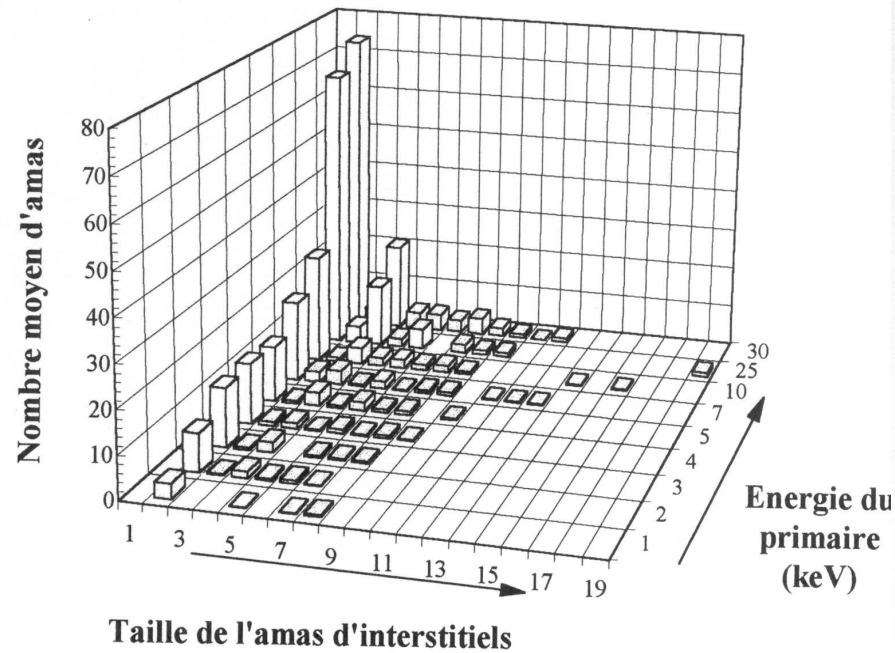
Cascade in Fe, 10 ps after the collision
Pka of 20 keV.
Molecular Dynamic Simulation

- Remains after 10 ps
- isolated Interstitials.
 - isolated vacancies.
 - Clusters of interstitials.
 - Clusters of vacancies.



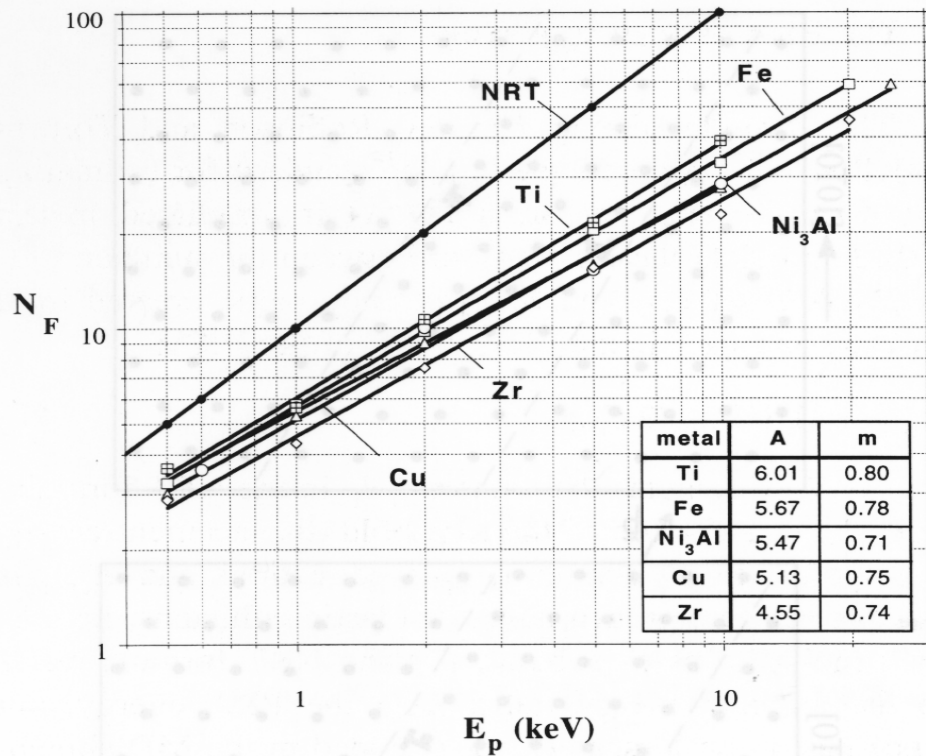
Défauts ponctuels et amas de défauts ponctuels dans les résidus

distribution of interstitial and vacancy clusters in cascades induced by primary iron ions (1 to 30 keV) in Fe (Vascon 1997)



A large portion of point defects is in the form of clusters

dpa DM versus dpa NRT



Le nombre de dpa donné par la dynamique moléculaire (DM) nettement inférieur aux dpa NRT

Quelques ordres de grandeur des taux de dommage

Réacteurs

	Flux neutrons $m^{-2}s^{-1}$ ($n > 1MeV$)	dpa_{NRT}/s	dpa_{NRT} fin de vie	T °C	Pb associés
REP éléments de coeur	10^{17}	$3 \cdot 10^{-8}$	qqs dpa	≤ 400	Internes : corrosion sous contrainte assistée par l'irradiation gaines : fluage, croissance, corrosion
REP Cuve	10^{15}	$3 \cdot 10^{-10}$	0.2	290	Fragilisation
RNR gaines	$3 \cdot 10^{18}$	10^{-6}	150	550	Gonflement

Particules chargées

Accélérateur d'ions	$10^{-3} - 10^{-5} dpa_{NRT}/s$
Microscope électronique à haute tension (électrons)	$10^{-3} - 10^{-5} dpa_{NRT}/s$
Accélérateur d'électrons	$10^{-9} dpa_{NRT}/s$

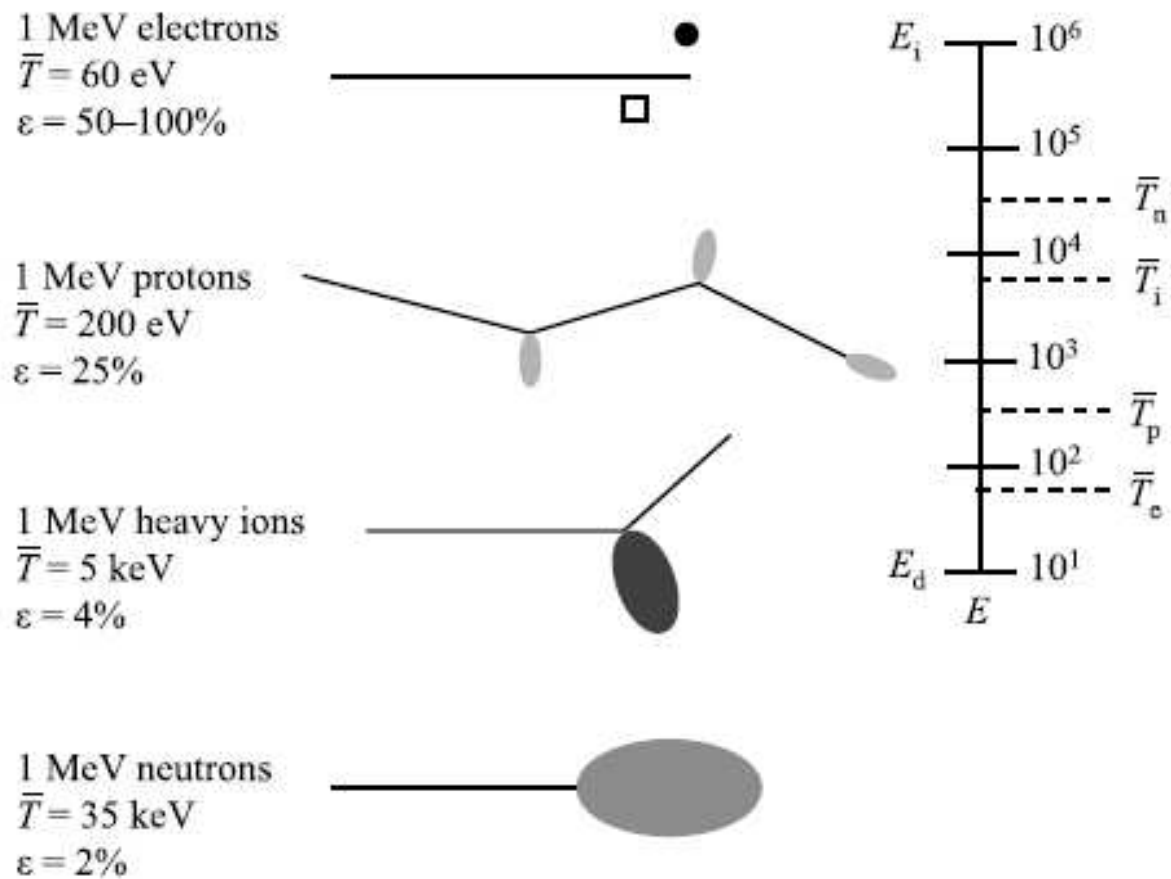
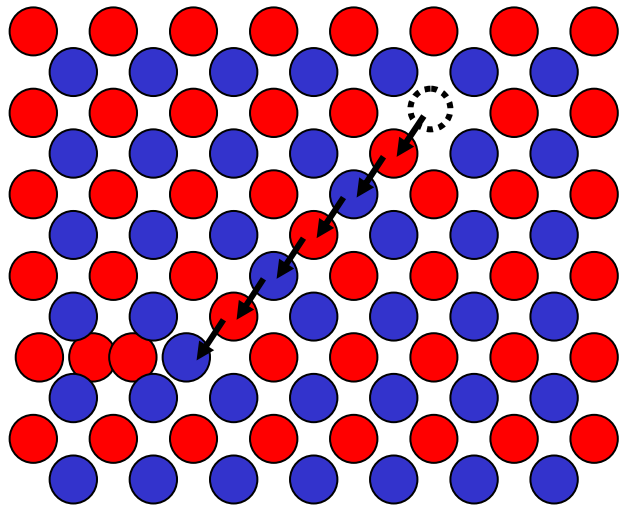


Fig. 3.7. Difference in damage morphology, displacement efficiency and average recoil energy for 1 MeV particles of different type incident on nickel (after [6])

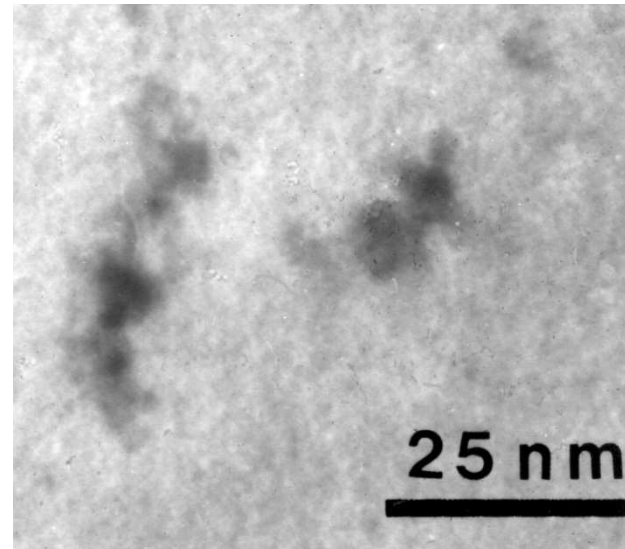
Effet du dommage ballistique: Désordre chimique

Disorder

May be kept and observed at low temperature



Crowdion
=
chemical disorder in ordered alloys

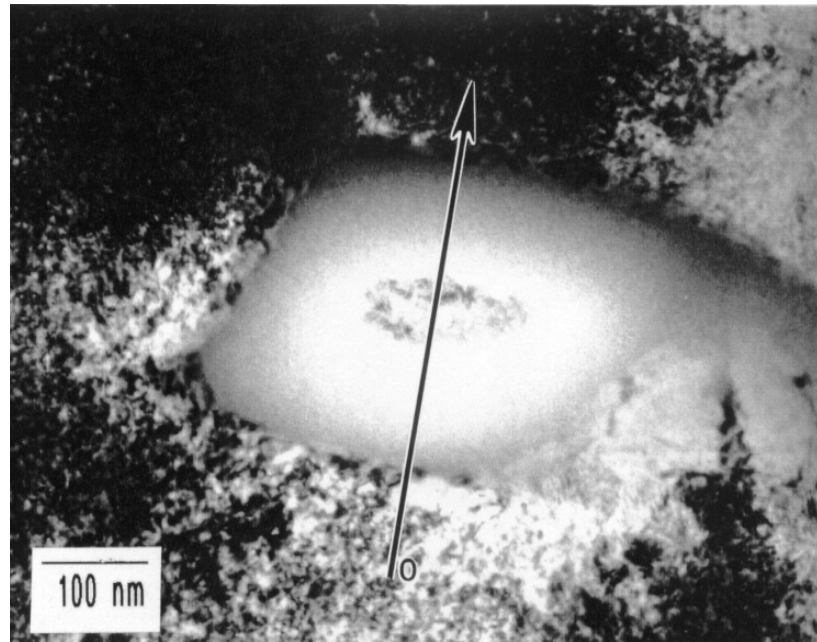


Disordered areas induced
by displacement cascades
in an ordered Cu_3Au alloy

Effet du dommage ballistique: Amorphisation

Lost of the crystalline structure in the cascade, for some compounds

Amorphisation under irradiation of $\text{Zr}(\text{Fe,Cr})_2$ precipitate in Zircaloy (Fe back to solution).



Cascades versus thermodynamique

Approximation

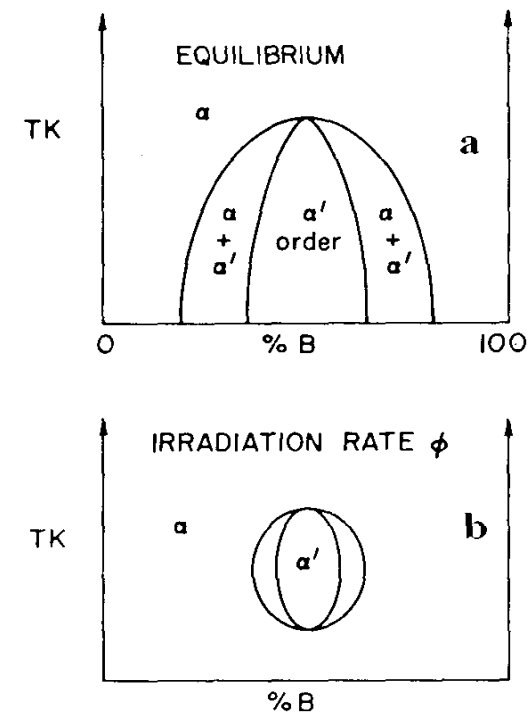
an alloy with clustering tendency will achieve under irradiation the macro state it would have outside irradiation at a higher effective temperature

T_{eff}

$$T_{\text{eff}} = T \left(1 + \frac{D^{\text{bal}}}{D_{\text{ch}}} \right)$$

In alloy with ordering tendency, owing to the flux and temperature :
 enhancement of the ordering kinetic
 of a disordered solid solution
 (quenched) or disordering of an
 ordered alloy.

Modification of the phase diagram



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- Mobility

Slow evolution (secondary damage) :

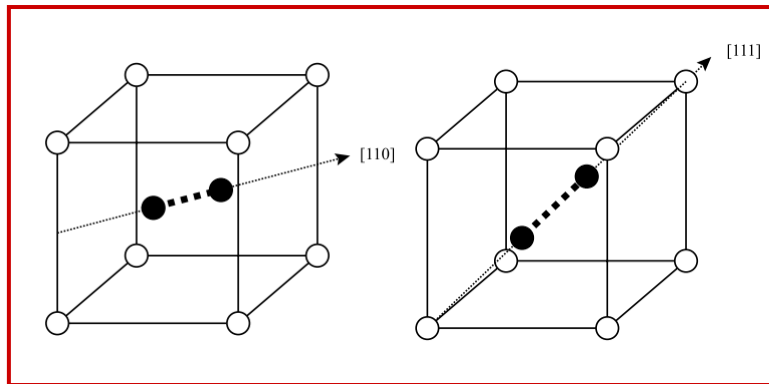
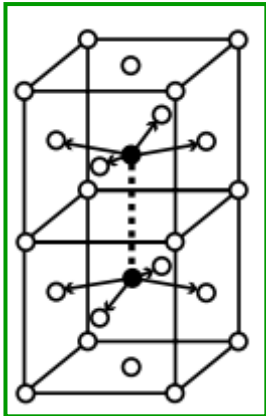
- Evolution of the point defects population:
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Macroscopic Consequences

Structure des défauts ponctuels

Interstitial

In compact structures (metals), for **Self Interstitial Atoms** (SIA), the stable configuration is N atoms sharing the same crystallographic site (**dumbbell** or **crowdion**) configuration.



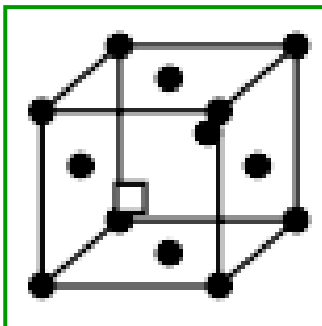
Energy of formation (E_f^i): **3 to 5 eV**

Relaxation Volume (V_r^i): **high**
($\sim 1.5 \Omega$)

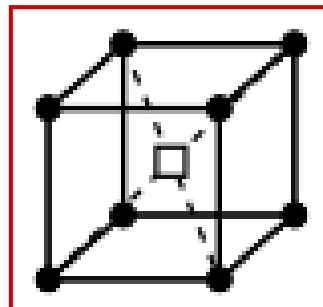
Vacancy

= empty crystallographic site

FCC



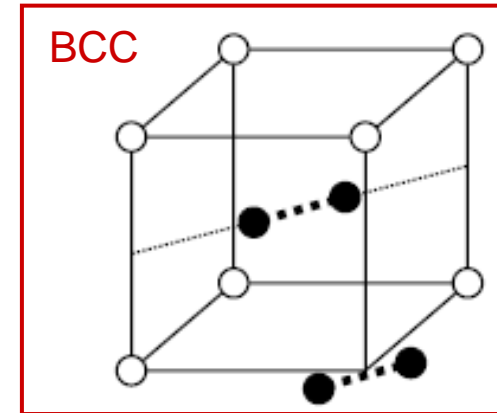
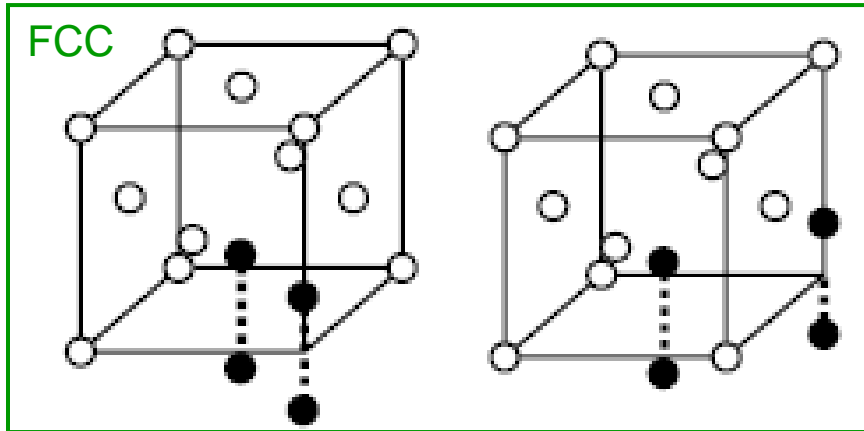
BCC



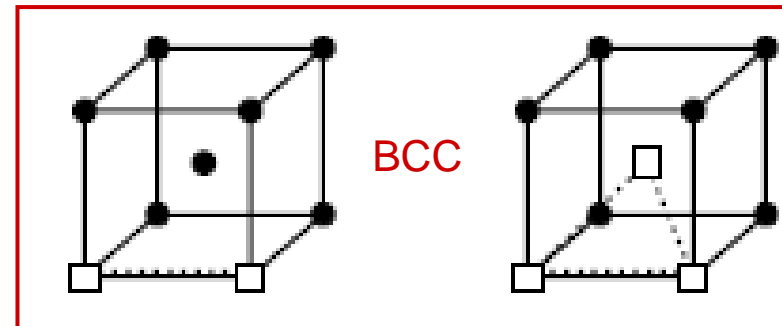
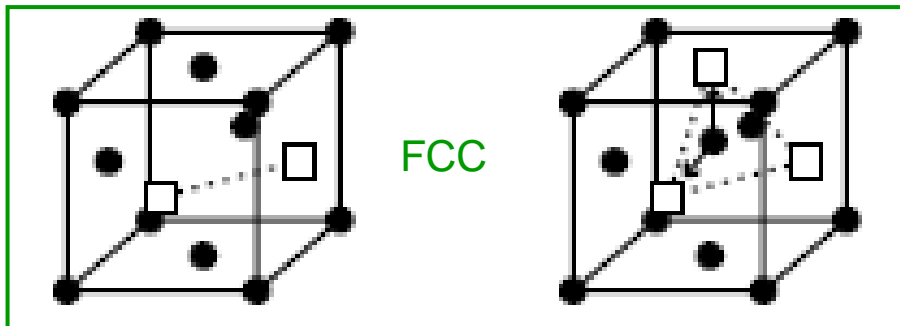
Energy of formation (E_f^v): **0.6 to 2 eV**
Relaxation Volume (V_r^v): **weak** (-0.2Ω)

Point defects and small clusters

Di-Interstitials

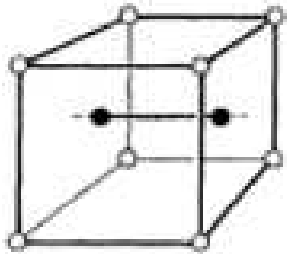


Di- and tri-vacancies

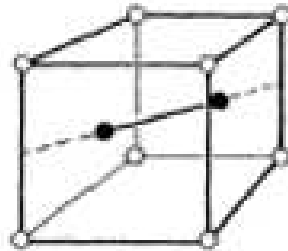


SIA dans Fe- α

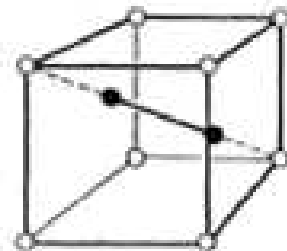
Configurations



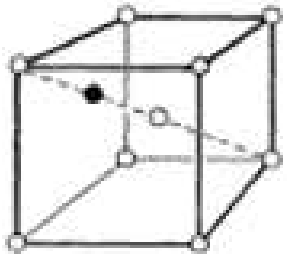
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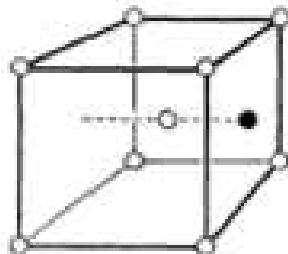
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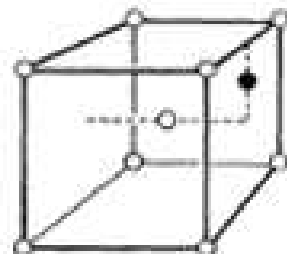
c



d



e

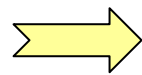
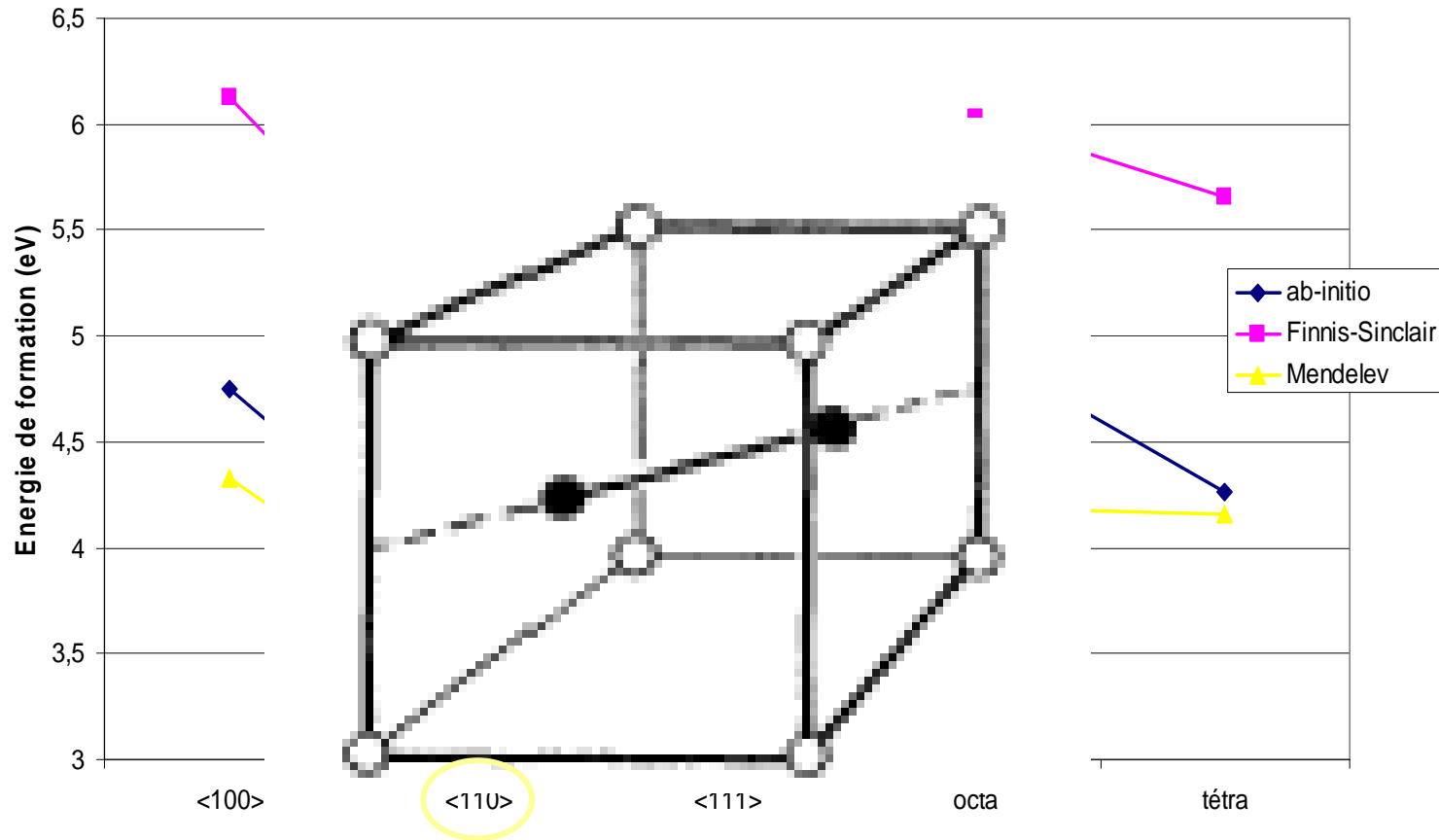


f

- a) $\langle 100 \rangle$ dumbbell
- b) $\langle 110 \rangle$ dumbbell
- c) $\langle 111 \rangle$ dumbbell
- d) $\langle 111 \rangle$ crowdion
- e) interstitiel octaédrique
- f) interstitiel tétraédrique

SIA dans Fe- α

Energie de formation des différentes configurations



Configuration la plus stable <110> dumbbell

Mécanismes de migration

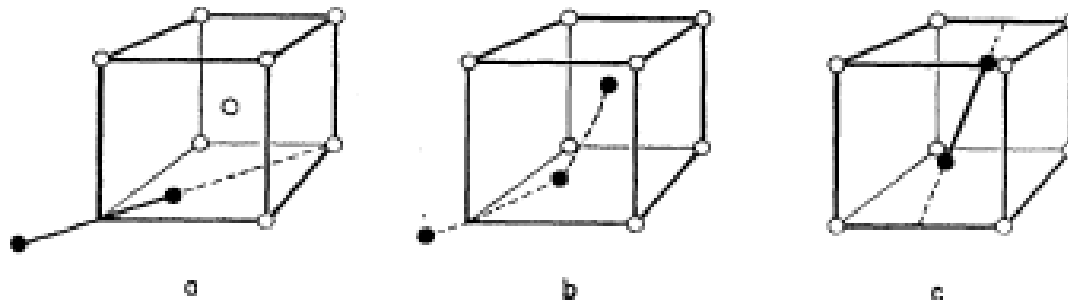
- Mécanisme de rotation/translation (DM)

- Rotation $\langle 110 \rangle \Rightarrow$ crowdion

- $(0,13 < E_m < 0,25 \text{ eV})$

- Translation $\langle 111 \rangle (\approx 0,04 \text{ eV})$

- Mécanisme de Johnson (Ab-initio)



$\langle 110 \rangle$ centré en $(0,0,0) \Rightarrow \langle 101 \rangle$ centré en $(1/2,1/2,1/2)$

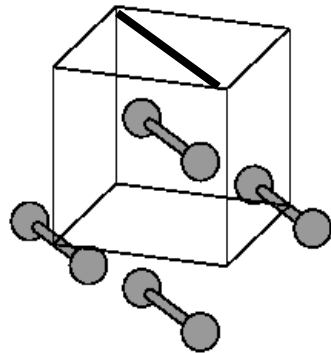
$(\approx 0,30\text{eV})$

Amas d'interstitiels dans Fe- α

Configuration

- n < 5:

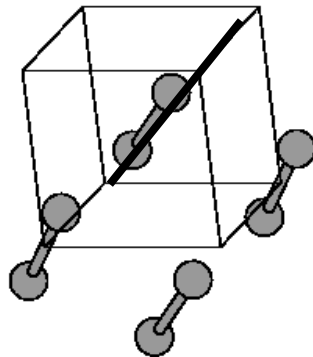
- **ab-initio** : ensemble de **dumbbells** $\langle 110 \rangle$ parallèles



Tétra-interstitiel $\langle 110 \rangle$ dumbbells

$$E_f = 11,05 \text{ eV}$$

- **DM** : ensemble de **crowdions** $\langle 111 \rangle$ parallèles



Tétra-interstitiel $\langle 111 \rangle$ crowdions

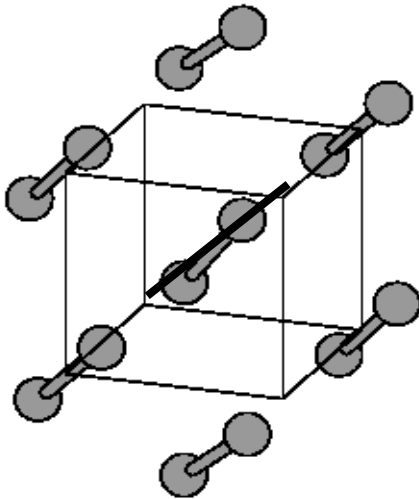
$$E_f = 14,4 \text{ eV (Wirth avec potentiel d'Ackland)}$$

Amas d'interstitiels dans Fe- α

Configuration

• $n \geq 5$:

- ab-initio et DM : ensemble de crowdions $\langle 111 \rangle$ parallèles



Hepta-interstitiel $\langle 111 \rangle$ crowdions

Ab-initio: $E_f = 16,6$ eV

DM : $E_f = 21,1$ eV

(Soneda avec potentiel de Johnson)

Travaux récents : C15 Laves structure

PRL 108, 025501 (2012)

PHYSICAL REVIEW LETTERS

week ending
13 JANUARY 2012

Irradiation-Induced Formation of Nanocrystallites with C15 Laves Phase Structure in bcc Iron

M.-C. Marinica, F. Willaime,* and J.-P. Crocombette

CEA, DEN, Service de Recherches de Métallurgie Physique, F-91191 Gif-sur-Yvette, France
(Received 28 September 2011; revised manuscript received 22 November 2011; published 11 January 2012)

A three-dimensional periodic structure is proposed for self-interstitial clusters in body-centered-cubic metals, as opposed to the conventional two-dimensional loop morphology. The underlying crystal structure corresponds to the C15 Laves phase. Using density functional theory and interatomic potential calculations, we demonstrate that in α -iron these C15 aggregates are highly stable and immobile and that they exhibit large antiferromagnetic moments. They form directly in displacement cascades, and they can grow by capturing self-interstitials. They thus constitute an important new element to account for when predicting the microstructural evolution of iron base materials under irradiation.

DOI: 10.1103/PhysRevLett.108.025501

PACS numbers: 61.72.Bb, 61.72.jj, 61.80.Az, 61.82.Bg

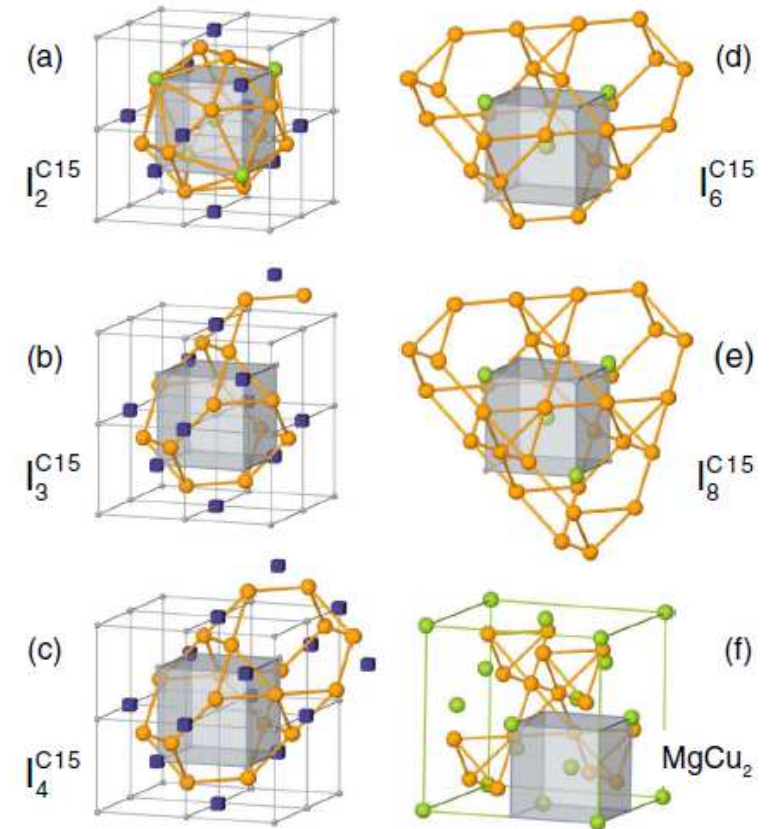
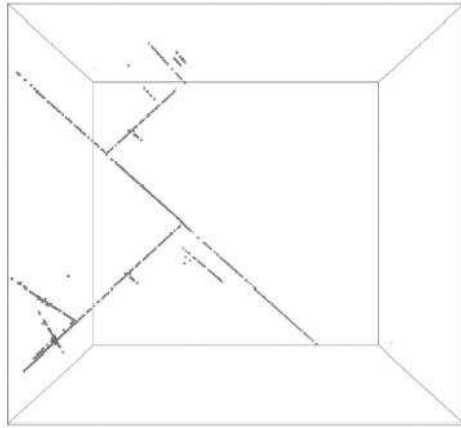


FIG. 1 (color online). Structure of small C15 interstitial clusters in the bcc lattice. (a)–(c) Representation by vacancies (blue cubes) and interstitials (orange spheres) of the di-, tri-, and tetra-interstitial clusters. For the di-interstitial, the atoms of the bcc lattice at the center and at the edges of the Z16 Frank-Kasper polyhedron are also represented (green spheres). (d),(e) Skeleton representation, i.e., without the vacancies and the cubic lattice and with the atoms at the center of the Z16 polyhedra in green, of the hexa- and octa-interstitials. (f) Unit cell of the MgCu₂ C15 Laves structure, with the Mg atoms in green and the Cu atoms in orange. For every cluster with 3 SIAs or more, the variant with the lowest energy found within DFT in Fe is represented.

Amas d'interstitiels dans Fe- α

Migration

- $n < 4$:



- migration dans la direction $\langle 111 \rangle$ ($E_m < 0.1\text{eV}$)
- changement de direction par activation thermique ($E_{a2l} = 0,09\text{eV}$ et $E_{a3l} = 0,27\text{eV}$)

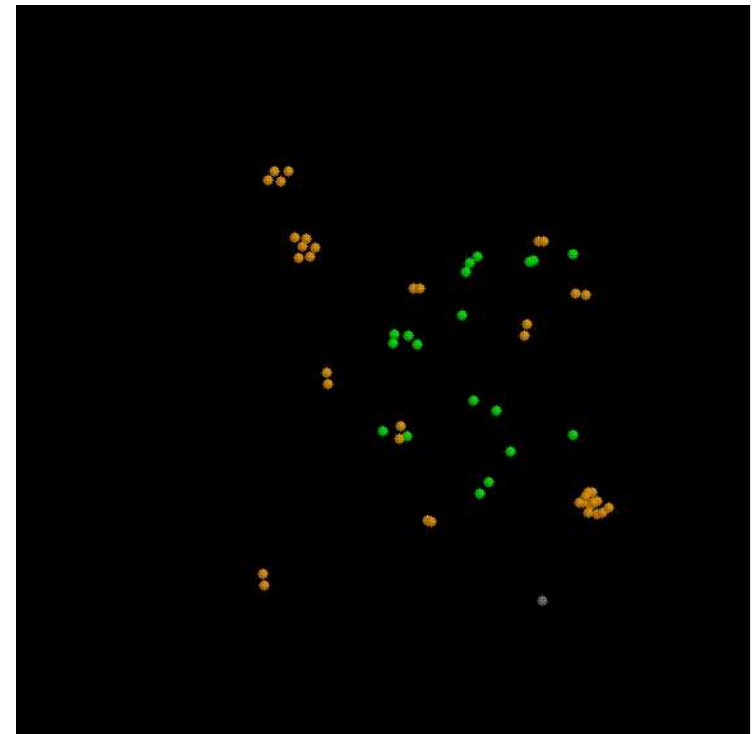
migration 1D/3D

Trajectoire d'un tri-interstitiel dans du fer- α à 1000K

- $n \geq 4$:

glissement 1D dans la direction $\langle 111 \rangle$

➔ **migration 1D**



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Amas d'interstitiels dans Fe- α

Migration

		E_m (eV)	D_0 (cm ² .s ⁻¹)
Marian		$0,059 + 0,067 / n^{1,3}$	$8,98.10^{-3} n^{-0,61}$
Soneda		0,061	$4,6.10^{-4}$
Bacon		0,022-0,026	-
Wirth	n=19	0,023	$1,7.10^{-3}$
	n=37	0,052	$6,5.10^{-3}$
Osestky		0,02-0,05	-
Kuramoto n=200		0,2	-

➡ n=20 17cm < x < 68cm pendant 14 jours à 20°C

➡ n=200 0,95cm < x < 33cm pendant 14 jours à 20°C

Outline

Interaction ion-matter

Ballistic Damage (primary damage)

- Frenkel pairs
- Atomic Displacement Cascade
- Disorder induced by ballistic damage

Properties of point defects and their clusters :

- Structure
- Mobility

Slow evolution (secondary damage) :

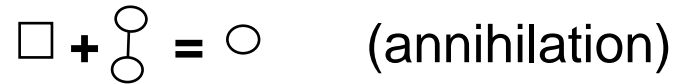
- Evolution of the point defects population:
- Consequence of the super-saturation of point defects
 - Agglomeration of point defects
 - Enhanced phase transformation
 - Induced Segregation and precipitation

Macroscopic Consequences

Evolution de la population de défauts ponctuels

Mécanismes fondamentaux

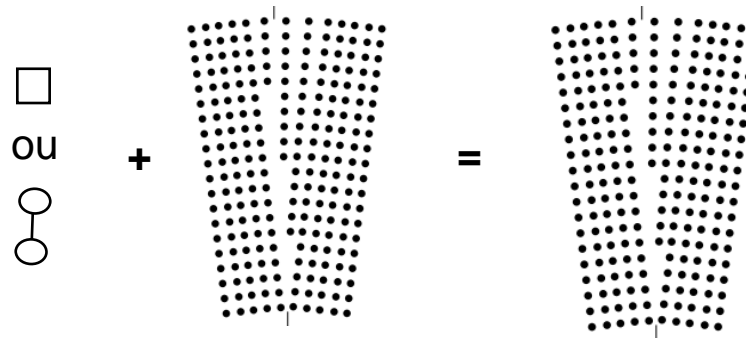
• Recombination



Recombination rate: $K_{iv} = 4\pi r_{iv} (D_i + D_v) \sim 4\pi r_{iv} D_i = R D_i$

• Elimination on sinks

- grain boundaries,
- free surfaces,
- dislocation lines,
- interfaces ...



interstitials: $i + s = s$
 $K_{is} = 4\pi r_{is} D_i$

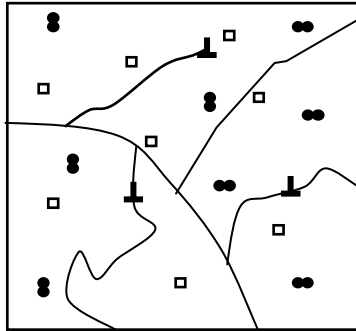
vacancies: $v + s = s$
 $K_{vs} = 4\pi r_{vs} D_v$

Evolution de la population de défauts ponctuels

Classical mean field approach
(*cinétique chimique homogène, rate equation, etc.*)

1/

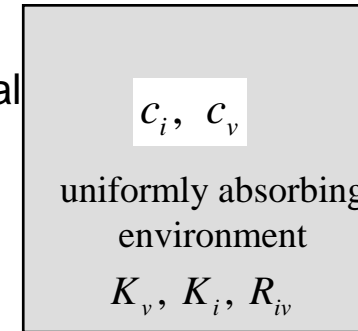
True environment



Homogeneous chemical
kinetic



Homogeneous environment



- / Isotrop system for the diffusion as in cubic structures
- / Constant concentration of sinks
- / Vacancies equilibrium concentration neglected

The homogeneous system is characterised by absorption coefficients where index j characterise the nature of the absorbing object

Equation bilan

creation recombination elimination on sinks

$$\frac{dC_v}{dt} = G - K_{iv} C_v C_i - K_{vs} C_v C_s$$

$$\frac{dC_i}{dt} = G - K_{iv} C_v C_i - K_{is} C_i C_s$$

or (equivalent to)

$$\frac{dC_v}{dt} = G - R D_i C_v C_i - K_v D_v C_v$$

$$\frac{dC_i}{dt} = G - R D_i C_v C_i - K_i D_i C_i$$

where

$$K_{vs} C_s = K_v D_v$$

$$K_{is} C_s = K_i D_i$$

with $K_\theta = \sum_s k_{\theta s}^2$

$k_{\theta s}^2 =$ strength of sink s on defect θ

Elimination on sink

The rate of elimination of point defects (DP) of α type on sink j is written when diffusion is the controlling process (not reaction at interface)

$$\left. \frac{\partial c_\alpha}{\partial t} \right|_j = -k_{j,\alpha}^2 D_\alpha c_\alpha$$

sink strength k_j^2 of an object j is given by $k_{j,\alpha}^2 = Z_{j,\alpha} Q_j$

Q_j capture rate

$Z_{j,\alpha}$ bias factor depend on the nature of PD

Expression of coefficients

Z is the bias factor (simple way to take into account the interaction)

Z=1 if no interaction taken into account

sink	Q	$Z_{n,\alpha}$
cavity	$4\pi r_c N_c Z_{c,\alpha}$	$Z_{c,i} = Z_{c,v} = 1$
Dislocation loop	$4\pi r_b N_b Z_{b,\alpha}$	$Z_{b,\alpha} = \frac{\pi}{\ln(8r_b / r_{p,\alpha})}$
dislocation	$\rho_d Z_{d,\alpha}$	$Z_{d,\alpha} = \frac{2\pi}{\ln \left\{ \frac{1}{r_{p,\alpha} (\pi \rho_d)^{1/2}} \right\}}$
Grain boundary	$\frac{57.6}{d^2}$	$Z_{gb,\alpha} = k'_\alpha d / 9.6$

Also, for Dislocations and dislocation loops : $Z_d^i > Z_d^v$

there is a stronger interaction for interstitial than vacancy because r_p is $\sim V_i^r > V_v^r$

$$Z_d^i \approx 1.1 ; 1.2$$

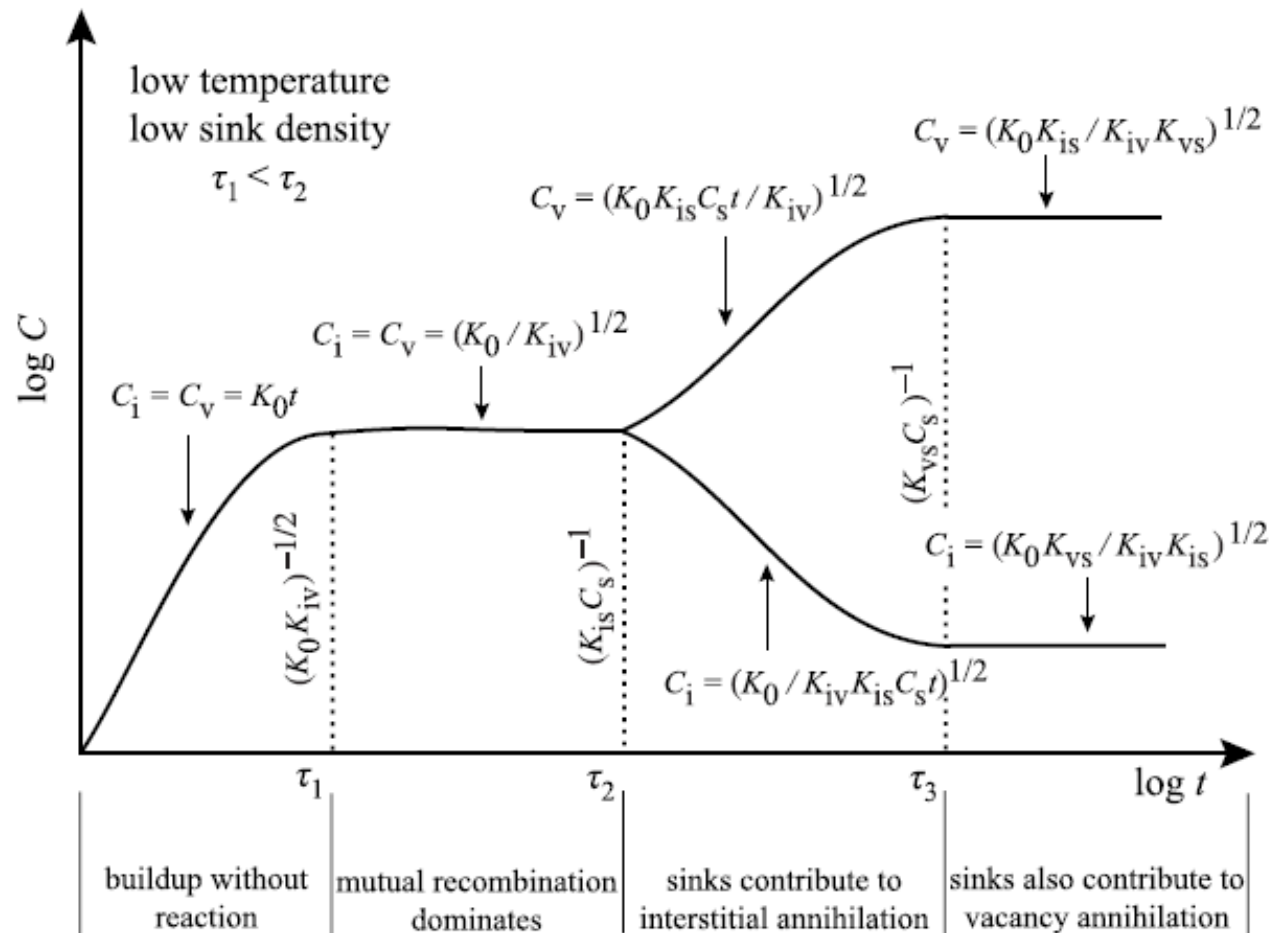
commonly used:

$$Z_d^v \approx 1$$

Cavities, grain boundaries and surfaces are neutral sinks (at first order): $Z^i = Z^v = 1$

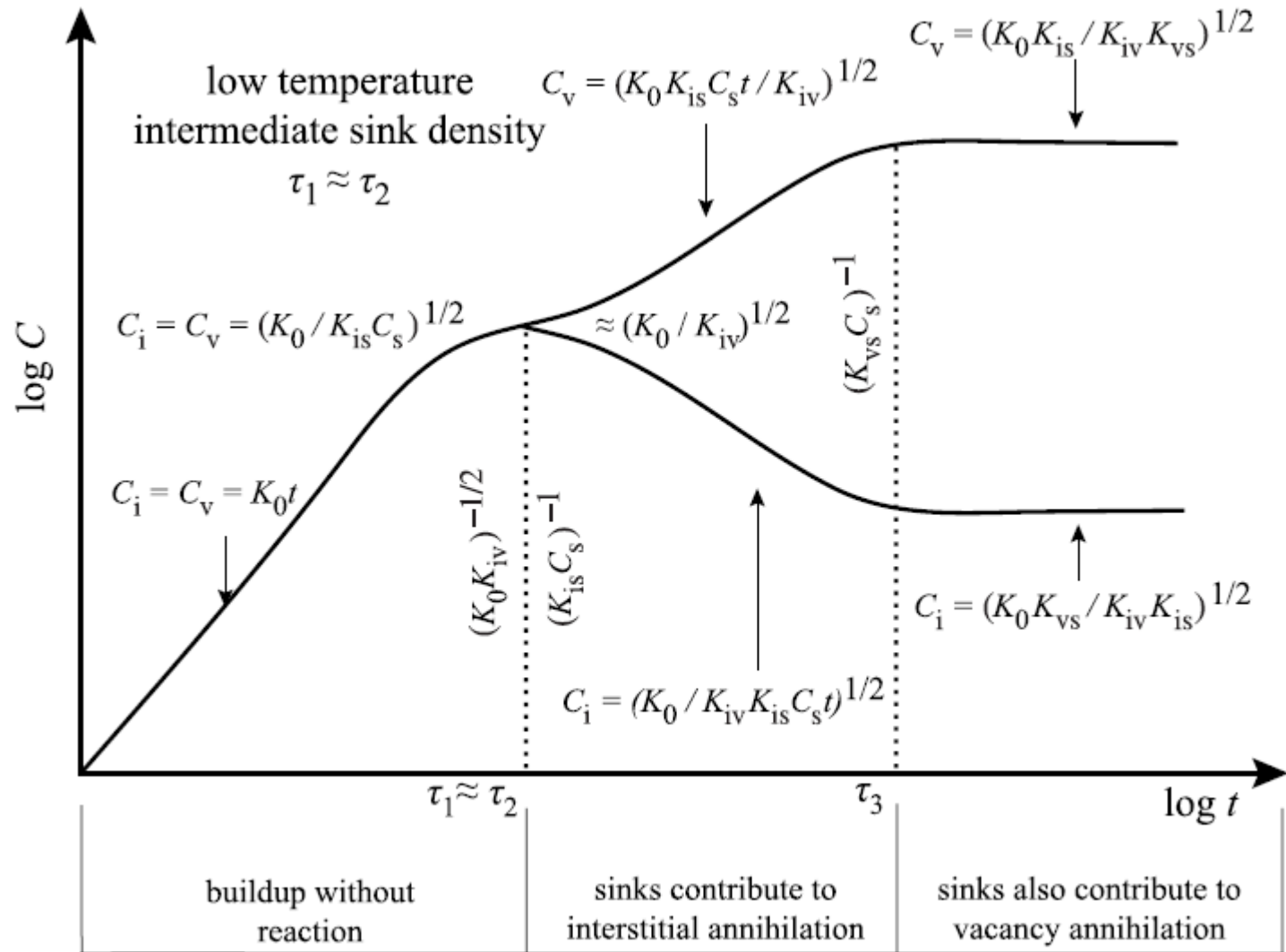
évolution de la population de défauts ponctuels

Low temperatures and low density of sinks



évolution de la population de défauts ponctuels

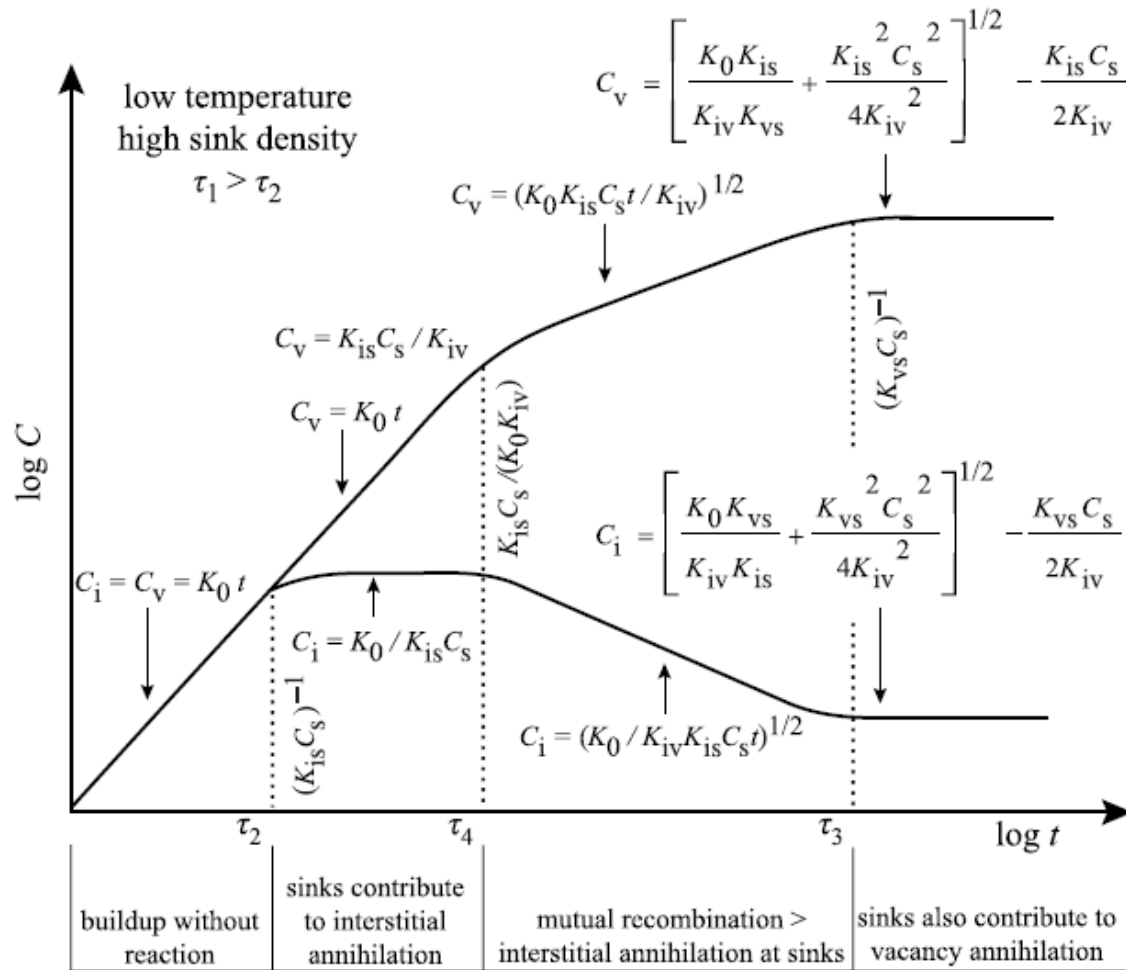
Low temperatures and intermediate density of sinks



$$G = K_0$$

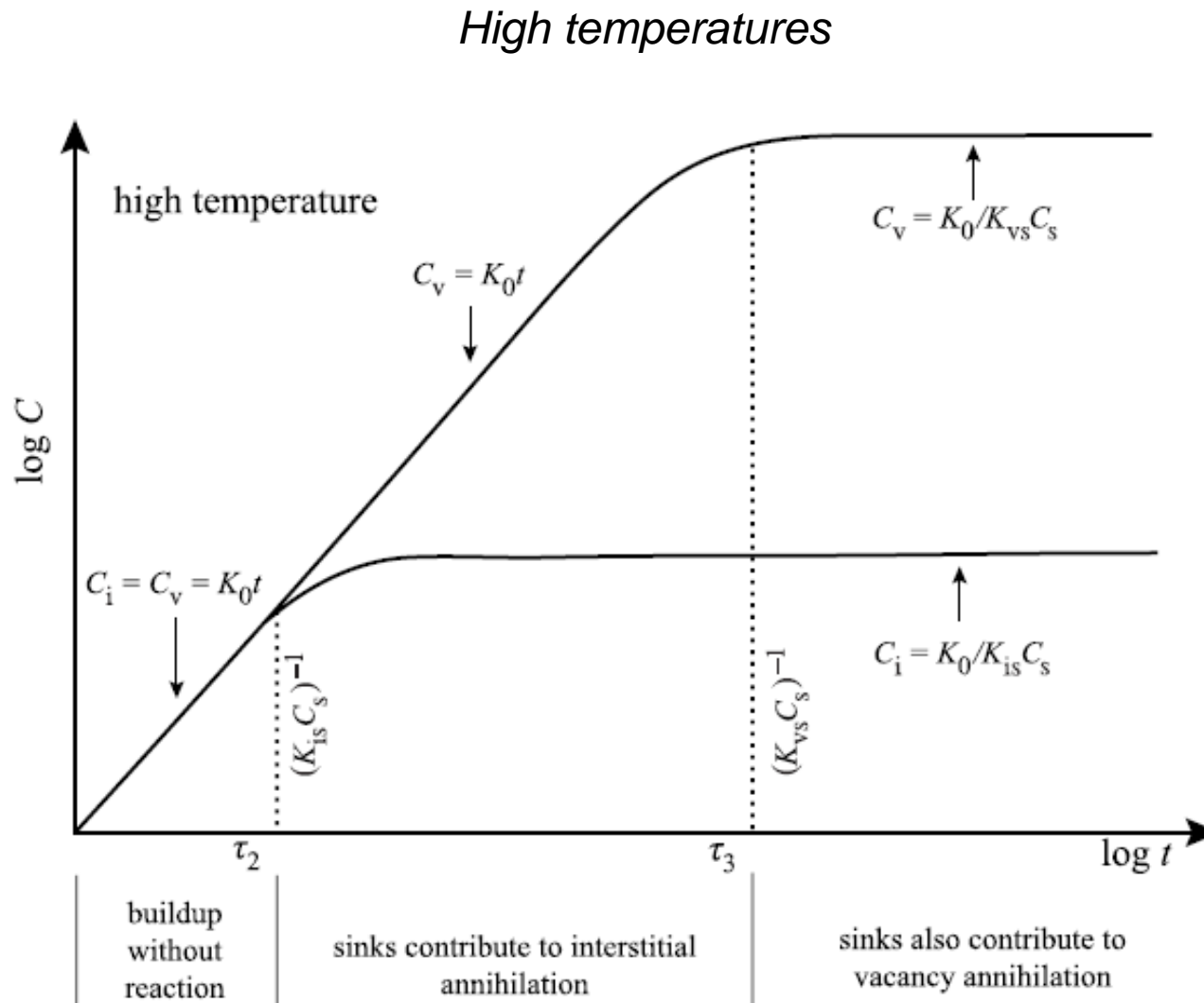
évolution de la population de défauts ponctuels

Low temperatures and high density of sinks
 $\tau_1 > \tau_2$



$$G = K_0$$

évolution de la population de défauts ponctuels



$$G = K_0$$

Examen...



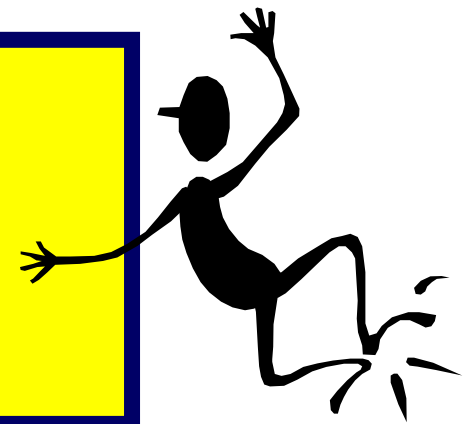
Calculez τ_3 dans le cas d'un réacteur à eau pressurisée
Hypothèse: on suppose que les puits sont majoritairement des dislocations avec $\rho=10^9\text{cm}^{-2}$.

Correction...

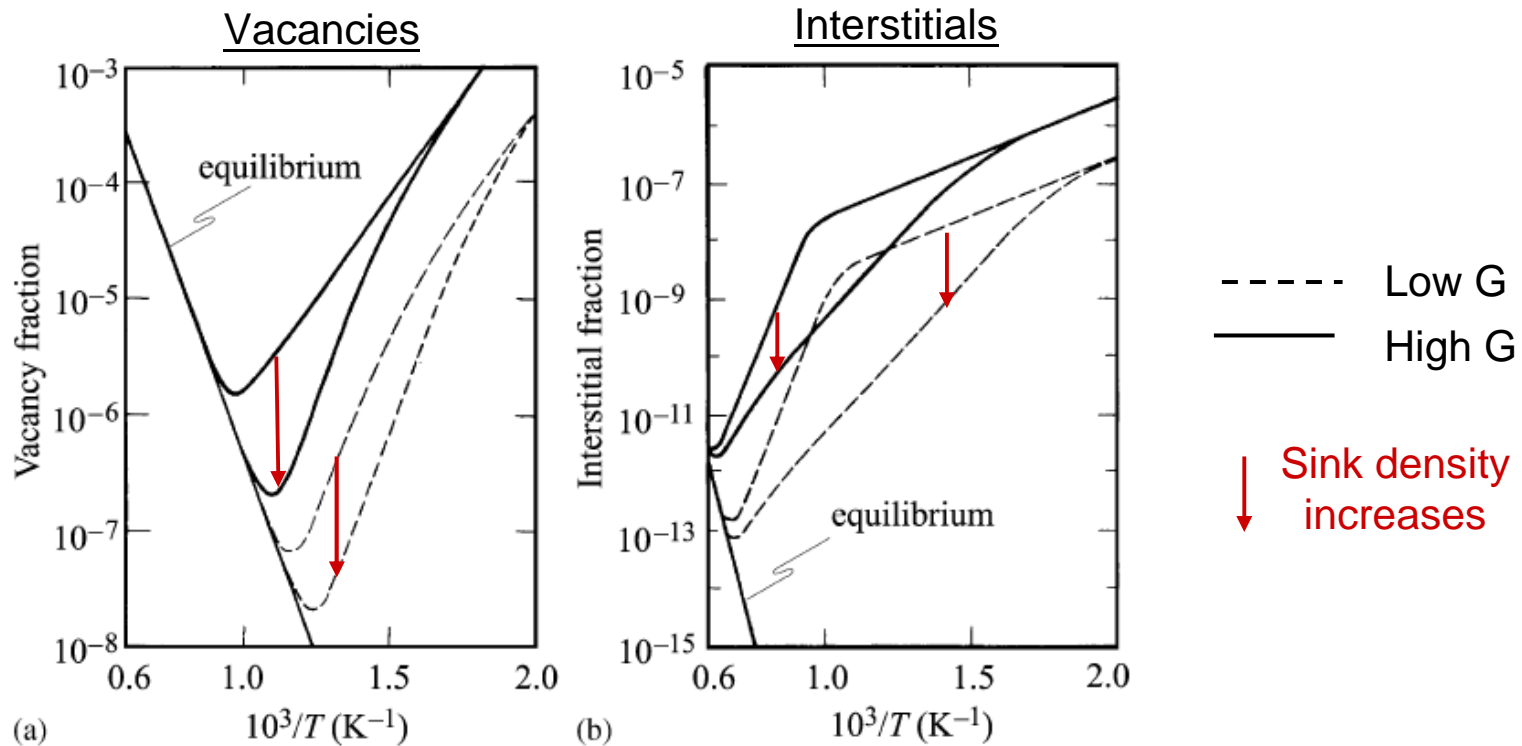
$$K_v^d = \rho Z_v^d = \rho$$

$$\tau_3 = 1/(3.5 \cdot 10^{-12} * 10^9) = 285s$$

Court en comparaison de la durée de vie...



Point defect concentration versus temperature



Three domains of temperature may be define:

High temperature

no irradiation effect

$$C_{\theta} = C_{\theta}^{eq}$$

Intermediate temperature

Elimination on sink dominant

$$c_v = \frac{G}{K_v D_v}$$

$$c_i = \frac{G}{K_i D_i}$$

Low temperature

Recombination dominant

$$c_v = \left(\frac{G K_i}{R K_v D_v} \right)^{1/2}$$

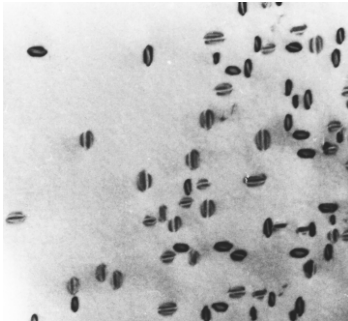
$$c_i = \left(\frac{G K_v D_v}{R K_i D_i^2} \right)^{1/2}$$

Défauts étendus (amas de défauts ponctuels)

- Agglomeration → defect clusters

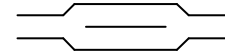
Interstitials (SIA)

dislocation loops in Ni

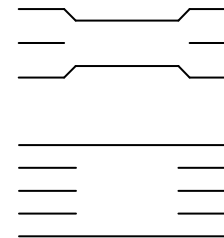


Dislocation loops (2D)

- Frank loops



- Perfect loops

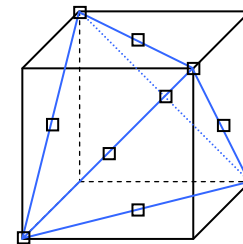


Vacancies

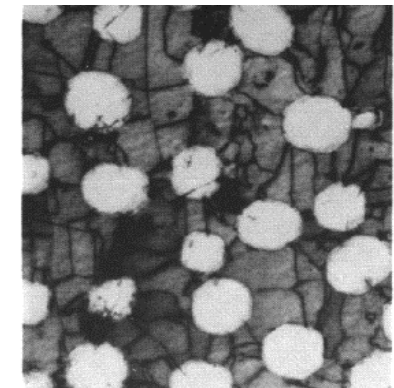
Dislocation loops (2D)

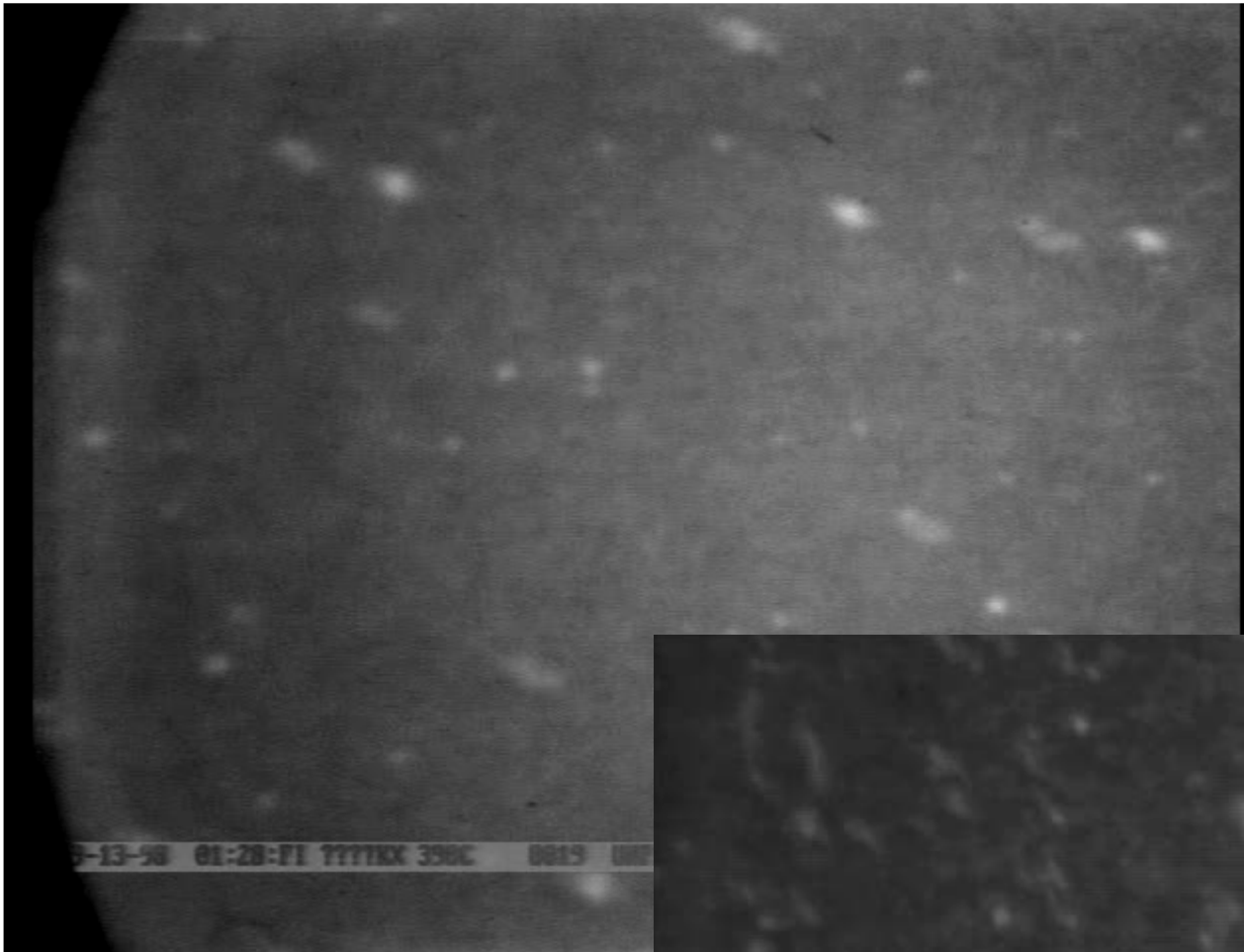
Cavities (3D)

Stacking Fault Tetrahedra (3D)

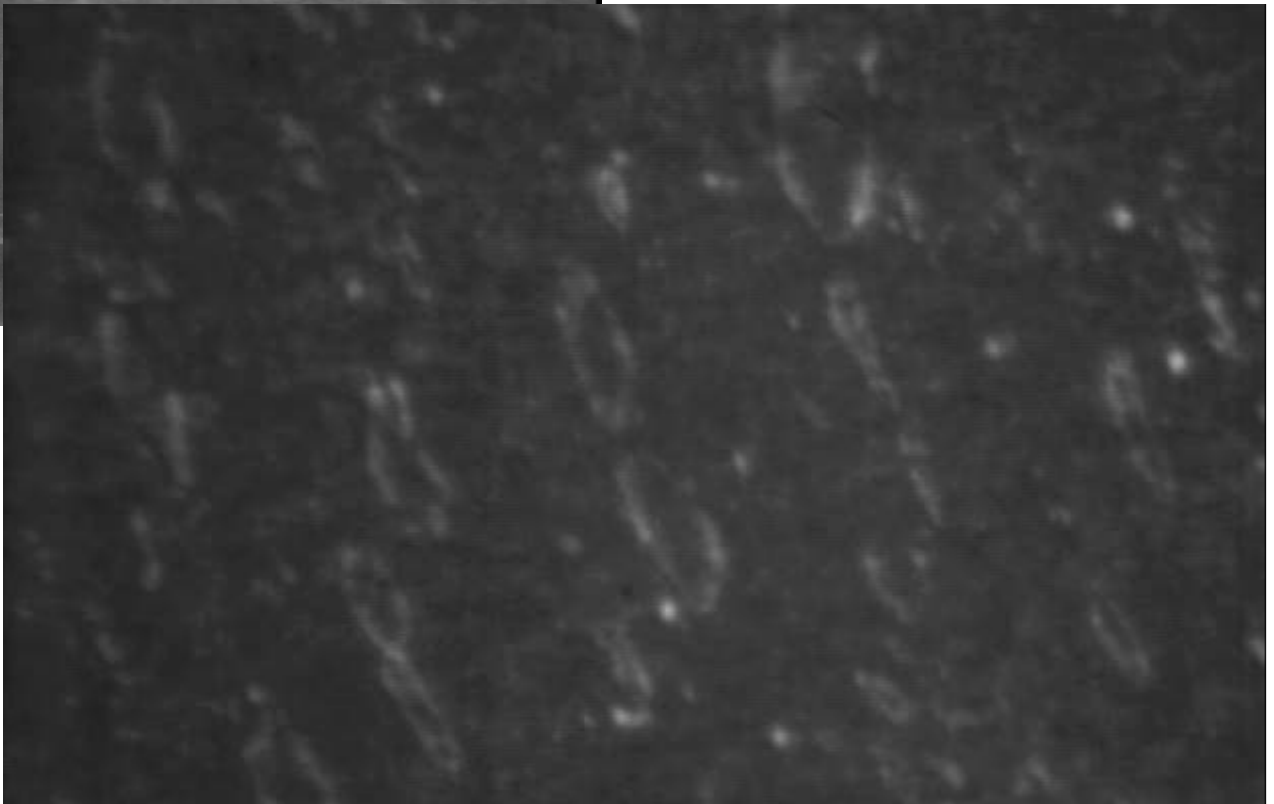


Cavity in Cu

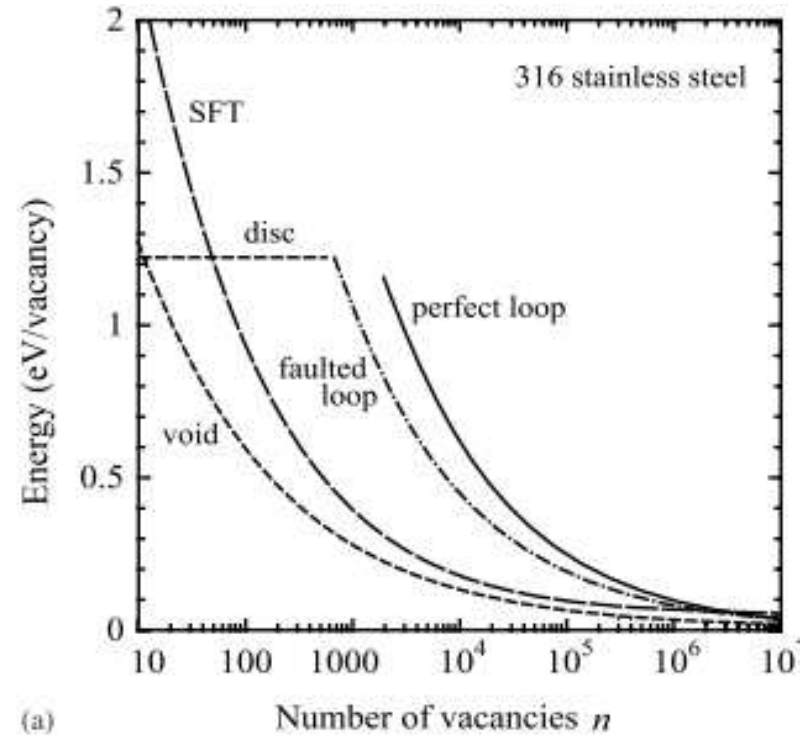
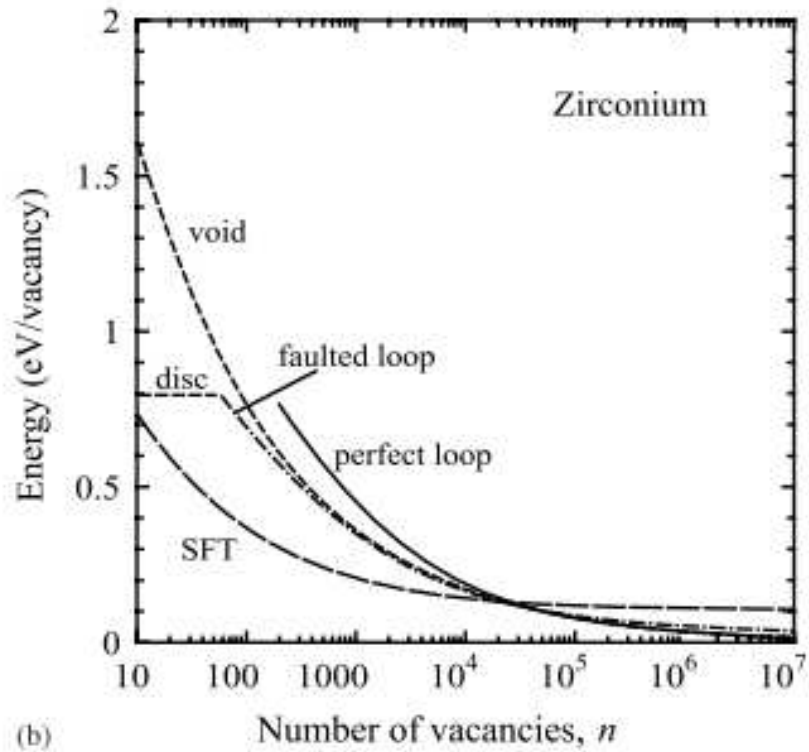




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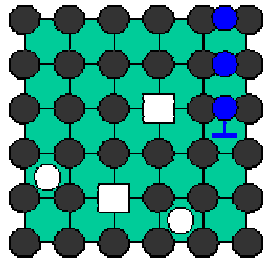
Extended Point defects Clusters



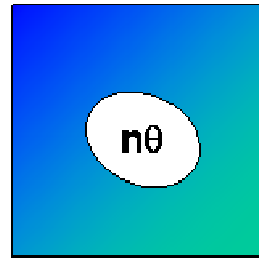
Evolution of point defects clusters

Classical mean field approach

True environment

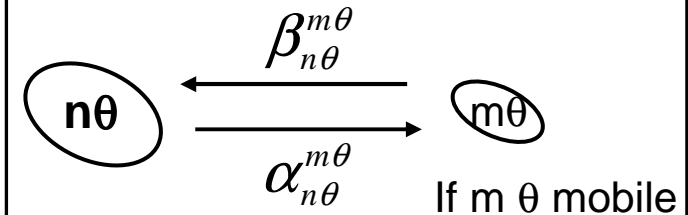


Homogeneous medium



$\theta = i \text{ or } v$

Consider reactions
between clusters



General equations (*hypo: only monomers are mobile*)

monomères

$$\frac{dC_{1\theta}}{dt} = \underbrace{G_{1\theta}} + \underbrace{\beta_{2\theta}^{1\theta'} C_{2\theta} C_{1\theta'} + 4\alpha_{2\theta}^{1\theta} C_{2\theta} + \sum_{n=3} (\alpha_{n\theta}^{1\theta} C_{n\theta})}_{\text{green}} - \underbrace{\sum_{n=2} (\beta_{n\theta}^{1\theta} C_{n\theta} + \beta_{n\theta}^{1\theta'} C_{n\theta'}) C_{1\theta} - 4\beta_{1\theta}^{1\theta} C_{1\theta} C_{1\theta}}_{\text{yellow}} - \underbrace{R_{iv} C_{1\theta} C_{1\theta'} - K_{1\theta}^d (C_{1\theta} - C_{1\theta}^{eq}) - K_{1\theta}^{sk} (C_{1\theta} - C_{1\theta}^{eq})}_{\text{red}}$$

dimères

$$\frac{dC_{2\theta}}{dt} = \underbrace{G_{2\theta}} + \underbrace{2\beta_{1\theta}^{1\theta} C_{1\theta} C_{1\theta} + \beta_{3\theta}^{1\theta'} C_{1\theta} C_{3\theta} + \alpha_{3\theta}^{1\theta} C_{3\theta}}_{\text{green}} - \underbrace{2\alpha_{2\theta}^{1\theta} C_{2\theta} - \beta_{2\theta}^{1\theta} C_{1\theta} C_{2\theta} - \beta_{2\theta}^{1\theta'} C_{1\theta} C_{2\theta}}_{\text{yellow}}$$

$n > 2$

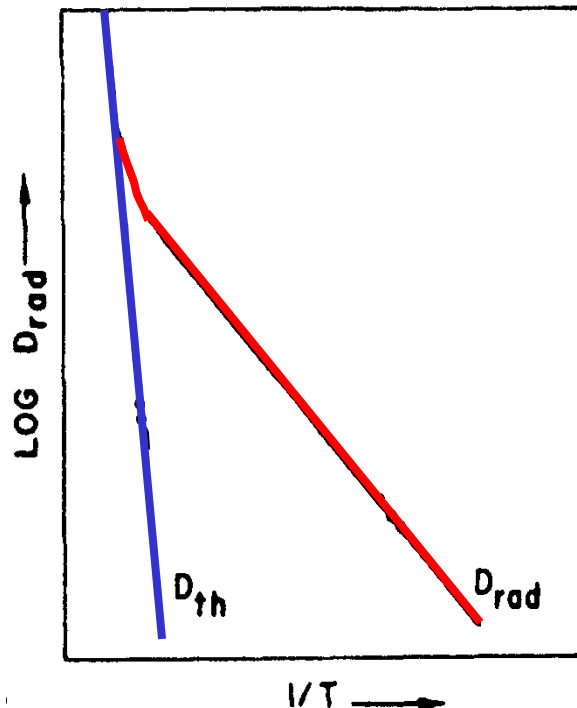
$$\frac{dC_{n\theta}}{dt} = \underbrace{G_{n\theta}} + \underbrace{\beta_{(n-1)\theta}^{1\theta} C_{1\theta} C_{(n-1)\theta} + (\beta_{(n+1)\theta}^{1\theta'} C_{1\theta'} + \alpha_{(n+1)\theta}^{1\theta}) C_{(n+1)\theta}}_{\text{green}} - \underbrace{(\alpha_{n\theta}^{1\theta} + \beta_{n\theta}^{1\theta} C_{1\theta} + \beta_{n\theta}^{1\theta'} C_{1\theta'}) C_{n\theta}}_{\text{yellow}}$$

Diffusion under irradiation

Diffusion of in pure metal

Theory of diffusion → $D^* = \alpha_v D_v C_v + \alpha_i D_i C_i$ α : correlation factor

- Excepted at high T, $C_v \gg C_v^{eq}$
- Diffusion via **interstitials only occurs under irradiation** ($C_i^{eq} \sim 0$)



→ Excepted at high T, $D^* \gg D^{th}$

= radiation enhanced diffusion

Ex: Cu in irradiated FeCu

$$D_{Cu}^{irrad} \approx D_v c_v = 3 \cdot 10^{-12} \times 3 \cdot 10^{-8} = 9 \cdot 10^{-20} \text{ cm}^2/\text{s}$$

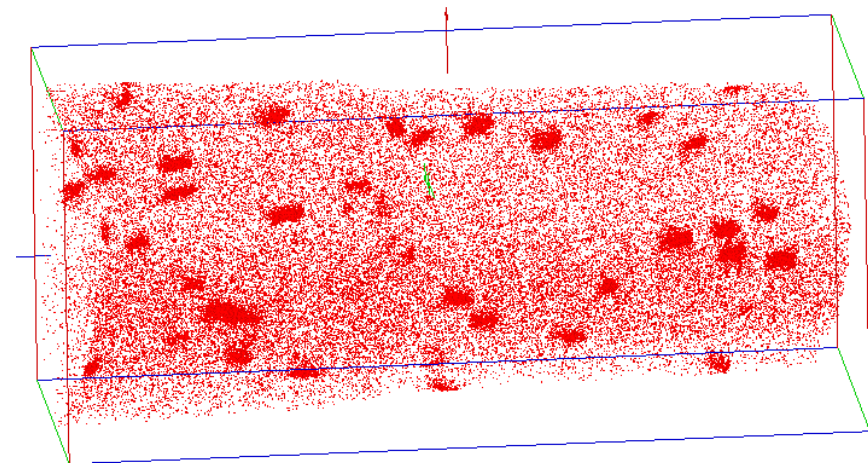
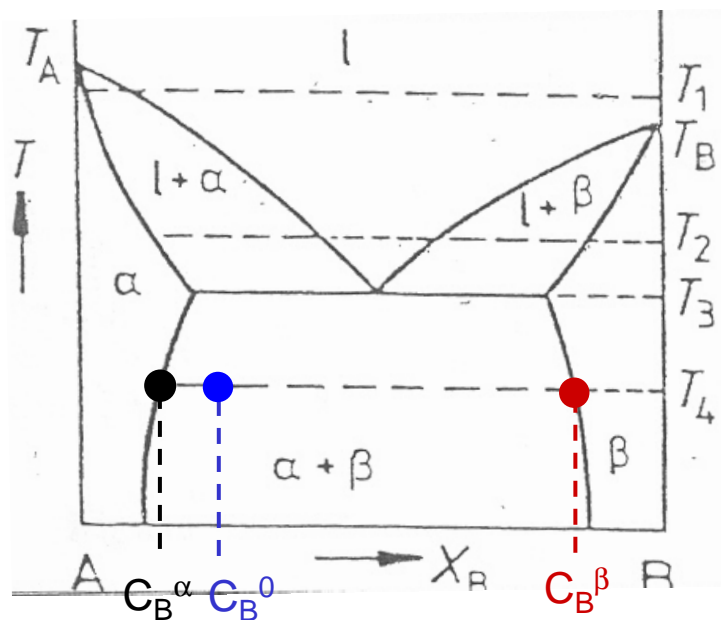
$$D_{Cu}^{th} = D_v c_v^e = 3 \cdot 10^{-12} \times 8 \cdot 10^{-16} = 2 \cdot 10^{-25} \text{ cm}^2/\text{s}$$

Irradiation enhanced precipitation

If cross coefficient can be neglected, the only effect of irradiation is to sustain a large defect supersaturation which:

- Increase the solute diffusion coefficient
- must **not modify the thermodynamic** of the system

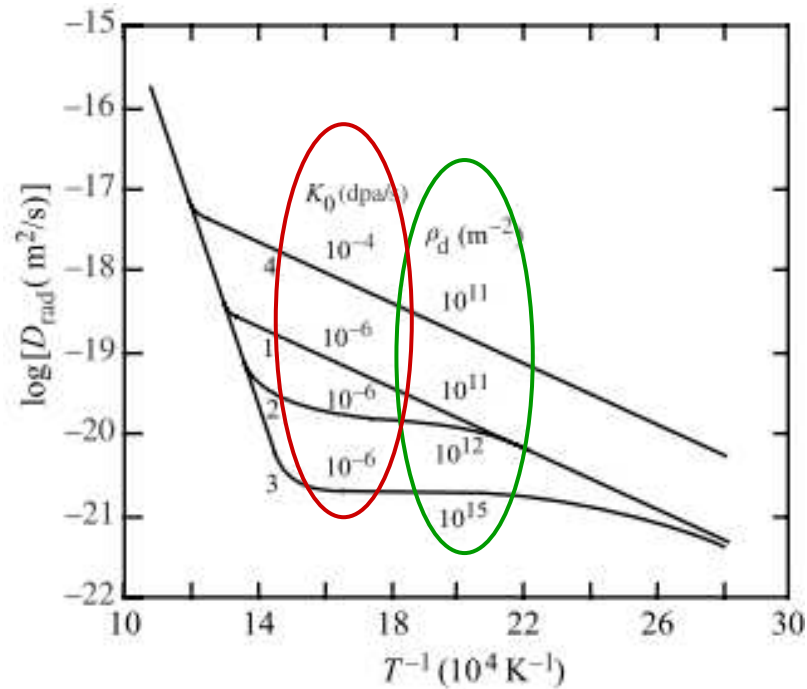
→ The **precipitation process will be accelerated**
= Irradiation enhanced precipitation



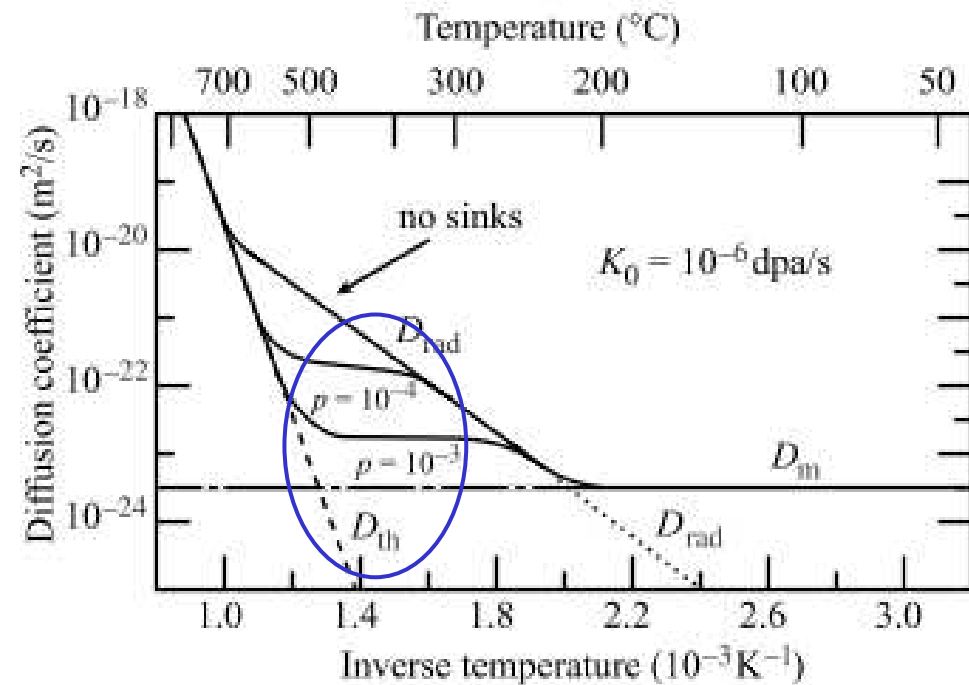
$$V = 45 \times 45 \times 100 \text{ nm}^3$$

Parameters influencing D^*

Self-diffusion of Cu



Ni-base irradiated at 10^{-6} dpa.s⁻¹

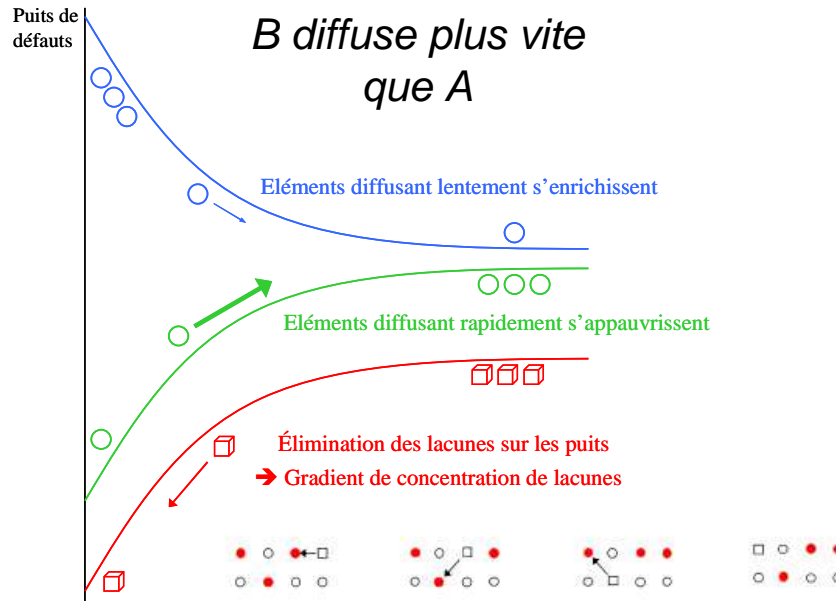


- **Dislocation density** (concentration of sinks)
- **Production rate**
- **Sink strength**

Solute transport under irradiation in AB alloy

Mécanismes lacunaire

(avec interaction B-v positive)

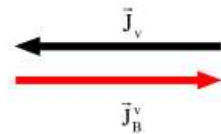


B diffuse plus vite que A

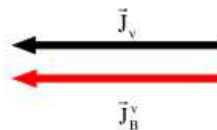
Eléments diffusant lentement s'enrichissent

Elément diffusant rapidement s'appauvrissent

Élimination des lacunes sur les puits
→ Gradient de concentration de lacunes

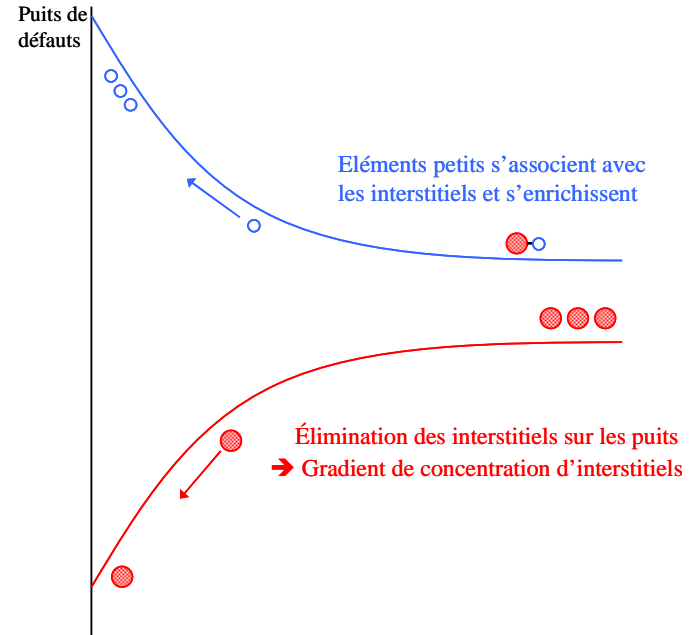


A diffuse plus vite que B



- Lacune
- Atome de soluté B
- Atome de solvant A

Mécanisme interstitiel



Eléments petits s'associent avec les interstitiels et s'enrichissent

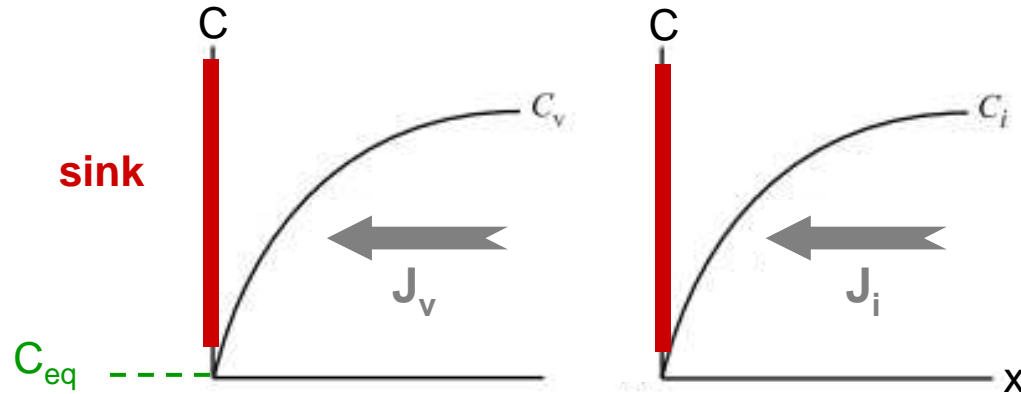
Élimination des interstitiels sur les puits
→ Gradient de concentration d'interstitiels

→ modification de la concentration locale au niveau du puits de défauts

$$\frac{\partial c_B}{\partial t} = -\text{div} \mathbf{J}_B$$

Solute transport under irradiation in AB alloy

Annihilation of point defects at sinks → **Gradient of concentration**



$$\frac{\partial c_i}{\partial t} = G - \text{div} \mathbf{J}_i - R D_i C_i C_v$$

$$\frac{\partial c_v}{\partial t} = G - \text{div} \mathbf{J}_v - R D_i C_i C_v$$

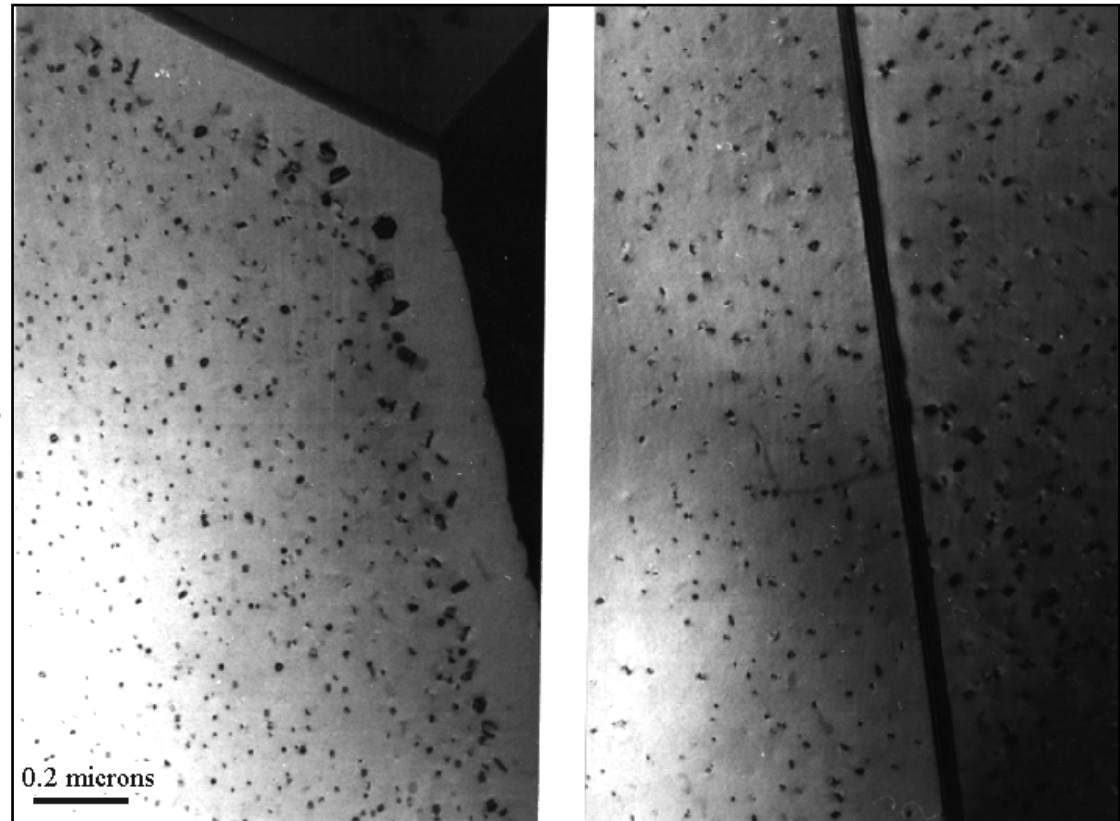
→ **Flux of point defects toward sinks**

By coupling, point defect fluxes result in a **flux of solute atoms (B)**

$$\begin{cases} \mathbf{J}_v = -\left(D_v \nabla c_v + d_{Bv} c_v \nabla c_B \right) \\ \mathbf{J}_i = -\left(D_i \nabla c_i + d_{Bi} c_i \nabla c_B \right) \\ \mathbf{J}_B = -\left(D_B \nabla c_B + c_B \left(d_{Bv} \nabla c_v + d_{Bi} \nabla c_i \right) \right) \end{cases}$$

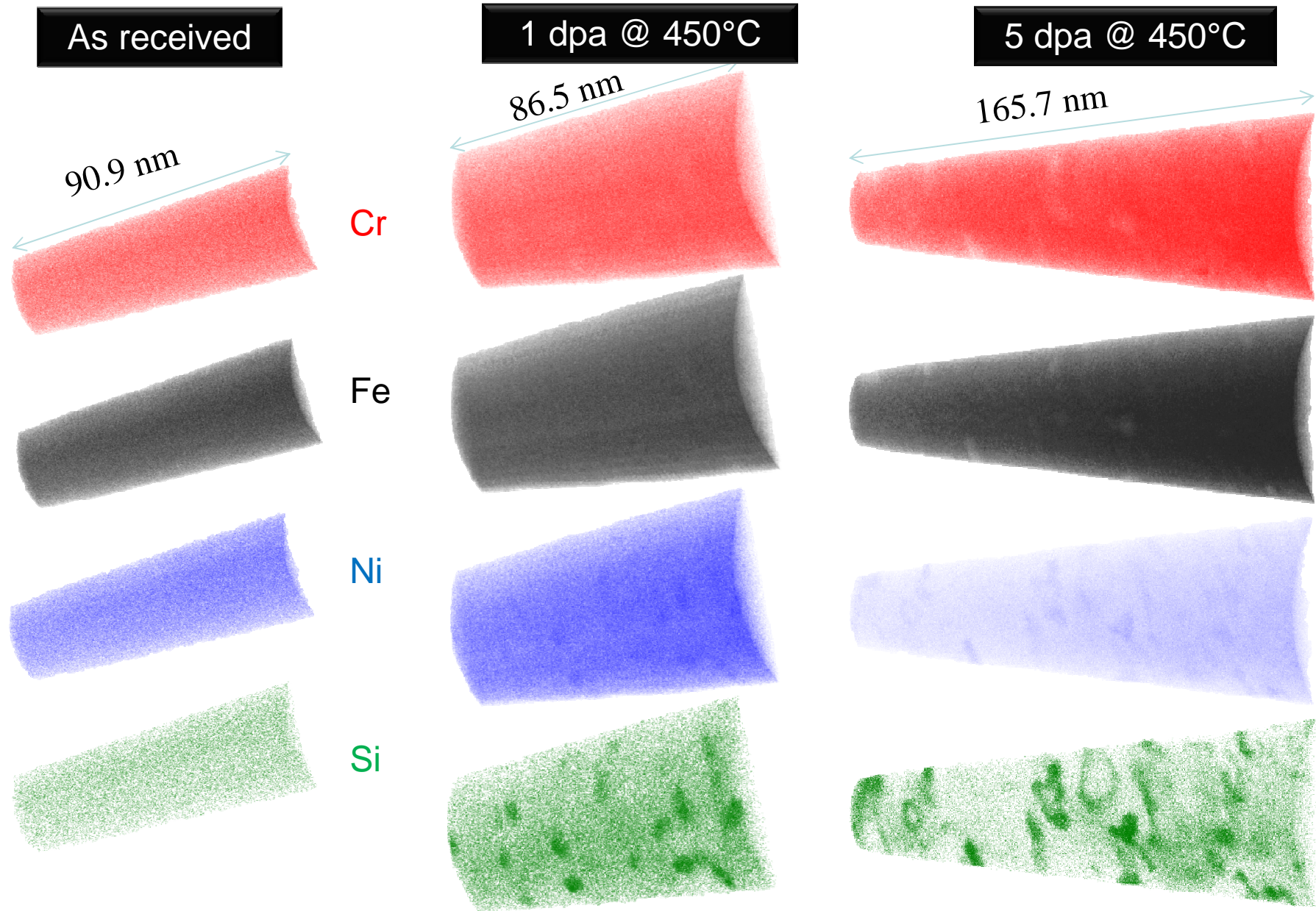
Zones dénudées au voisinage des joints de grains

- Les zones dénudées en défauts ponctuels se manifestent par l'existence de zones dénudées en boucles.
- Elles n'apparaissent pas pour tous les joints (L'efficacité des joints de grains pour l'élimination des défauts ponctuels dépend de leur nature).



Alliage à base de Nickel irradié avec des électrons de 2 MeV ($5 \cdot 10^{-9}$ dpa/s, 300°C, $8 \cdot 10^{-5}$ dpa).

FeNiCrSi model alloy : 5 MeV Ni⁺⁺



Outline

Interaction ion-matter

Ballistic Damage (primary damage)

- Frenkel pairs
- Atomic Displacement Cascade
- Disorder induced by ballistic damage

Properties of point defects and their clusters :

- Structure
- Mobility

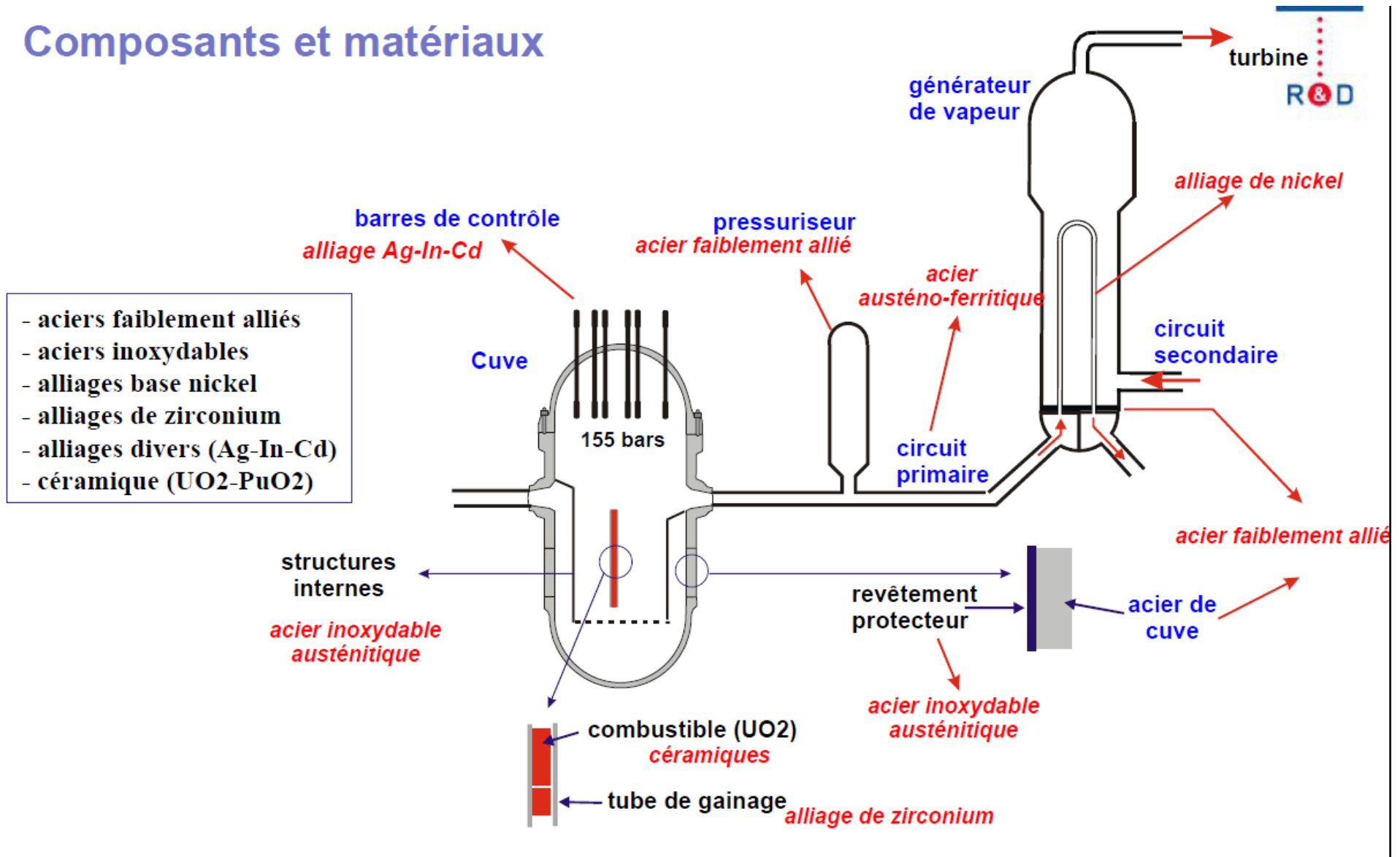
Slow evolution (secondary damage) :

- Evolution of the point defects population:
- Consequence of the super-saturation of point defects
 - Agglomeration of point defects
 - Enhanced phase transformation
 - Induced Segregation and precipitation

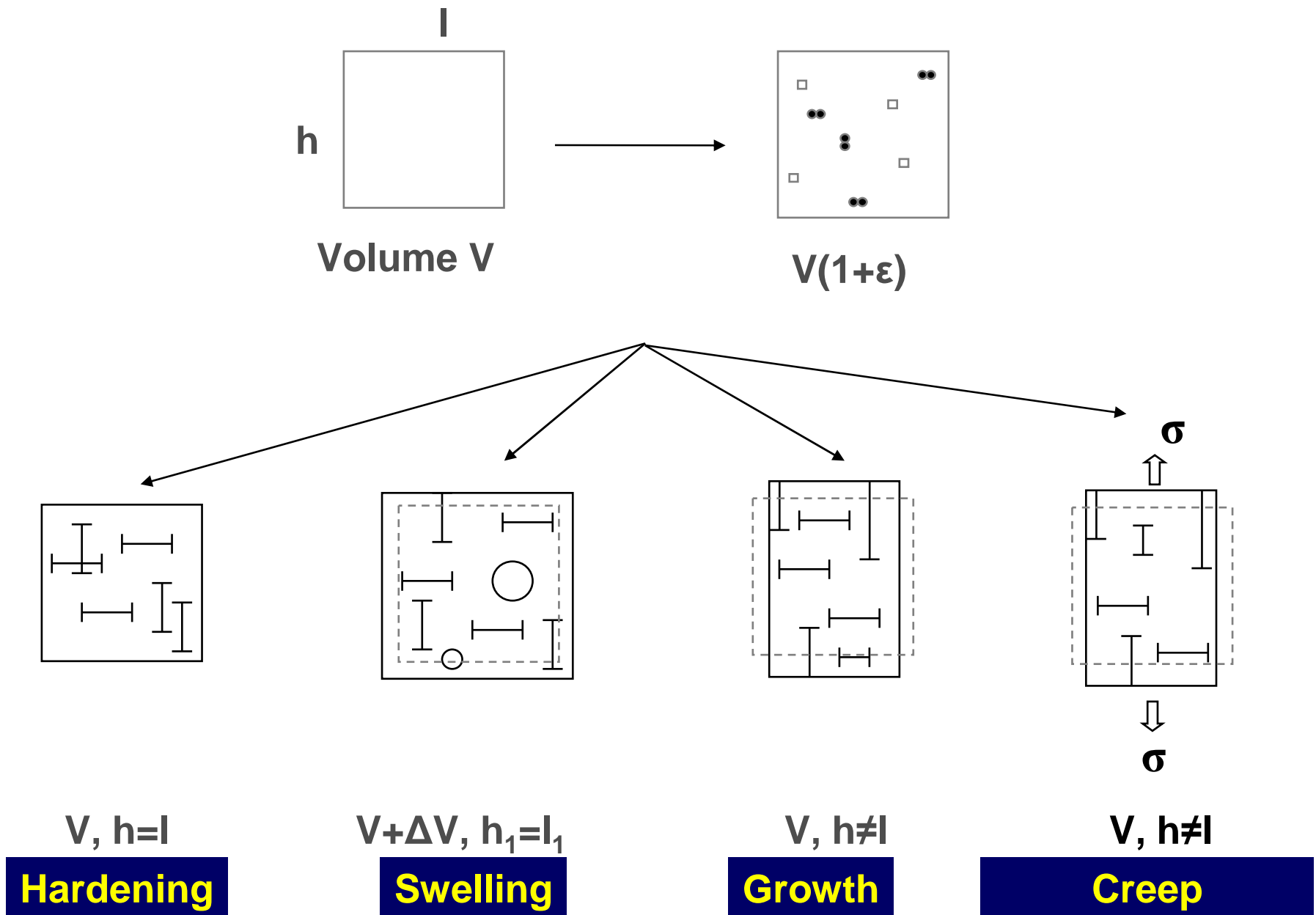
Macroscopic Consequences

Chaque Matériau est un cas particulier

Composants et matériaux

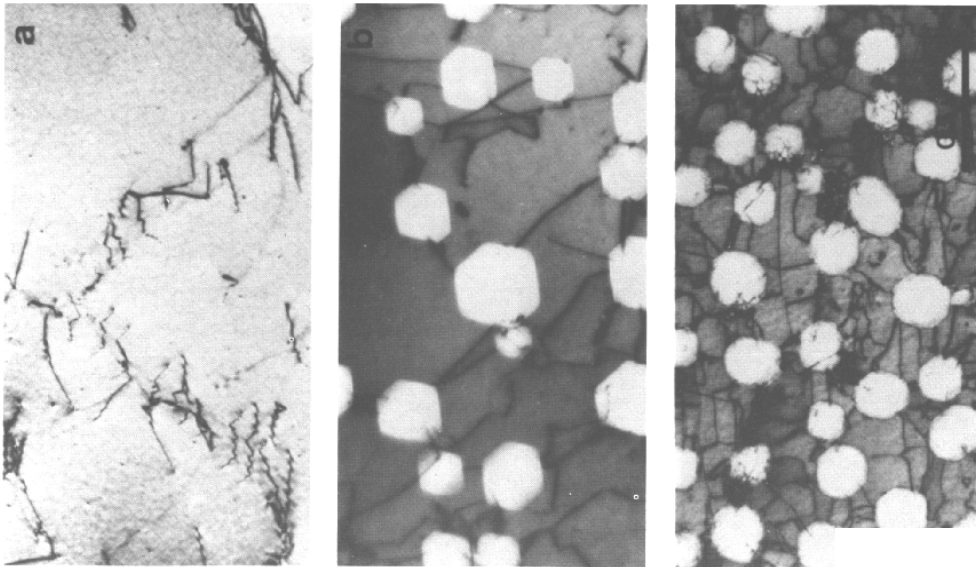


Dimensional variations



Swelling

Only happen when the vacancy flux towards cavities is more important than the interstitial one



500°C irradiation with Cu ions of
500 keV at $3 \cdot 10^{-3}$ dpa/s;
Oxygen 30, 70 et 110 ppm
(Glowinsky 1976)

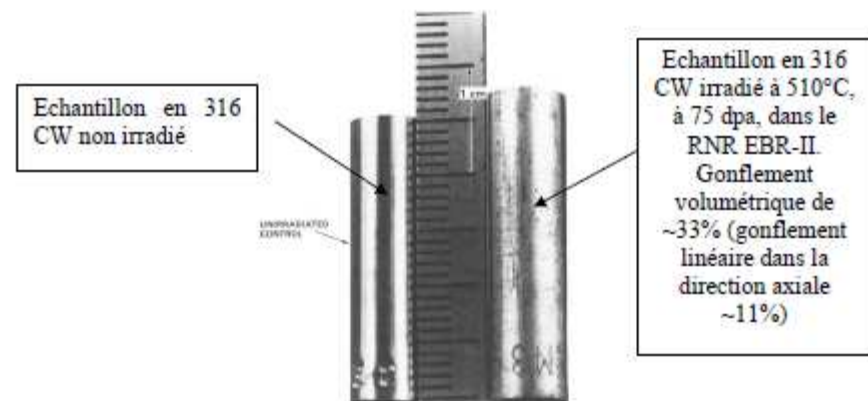
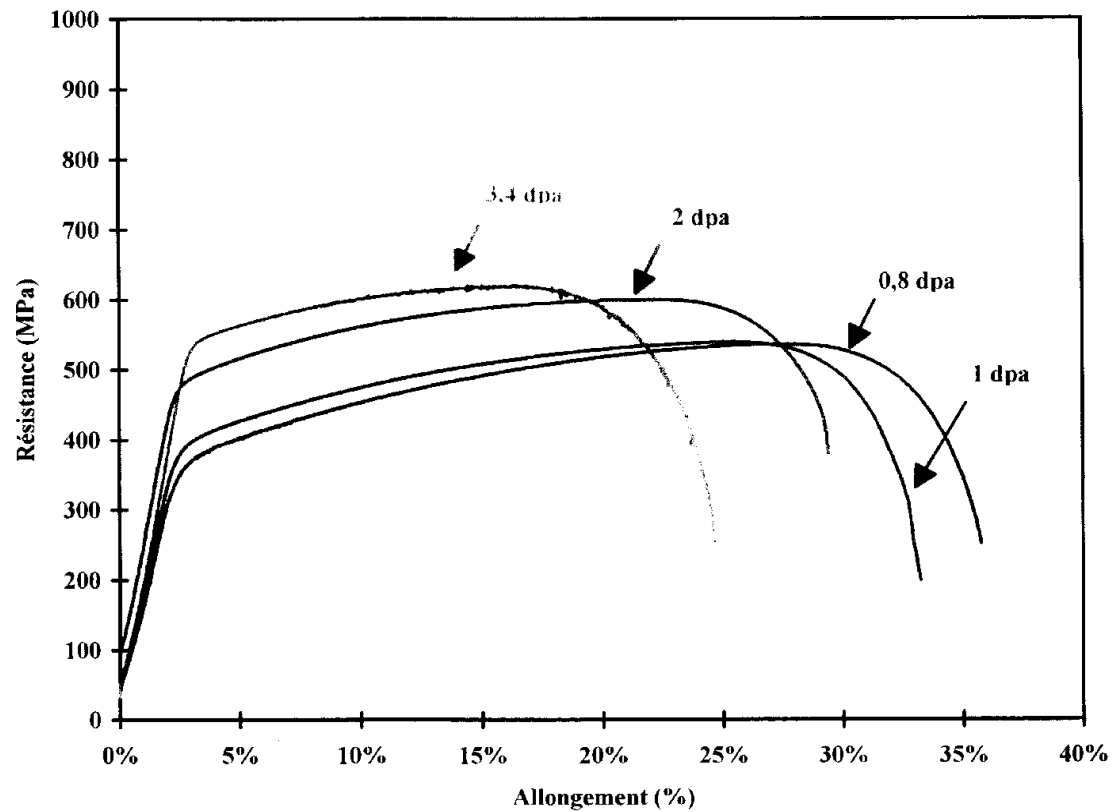


Figure I-20
Gonflement macroscopique de ~33% en volume, et ~11% en linéaire, observé dans un acier de type 316 CW, irradié à 510°C, à 75 dpa dans le RNR EBR-II. L'échantillon à gauche est non irradié et celui de droite est irradié [77].

Hardening

- Increase of the tensile strength
- Decrease of the elongation.



Evolution des courbes de traction d'un acier austénitique (316) irradié avec des neutrons, à 325°C, en fonction de la fluence en dpa.

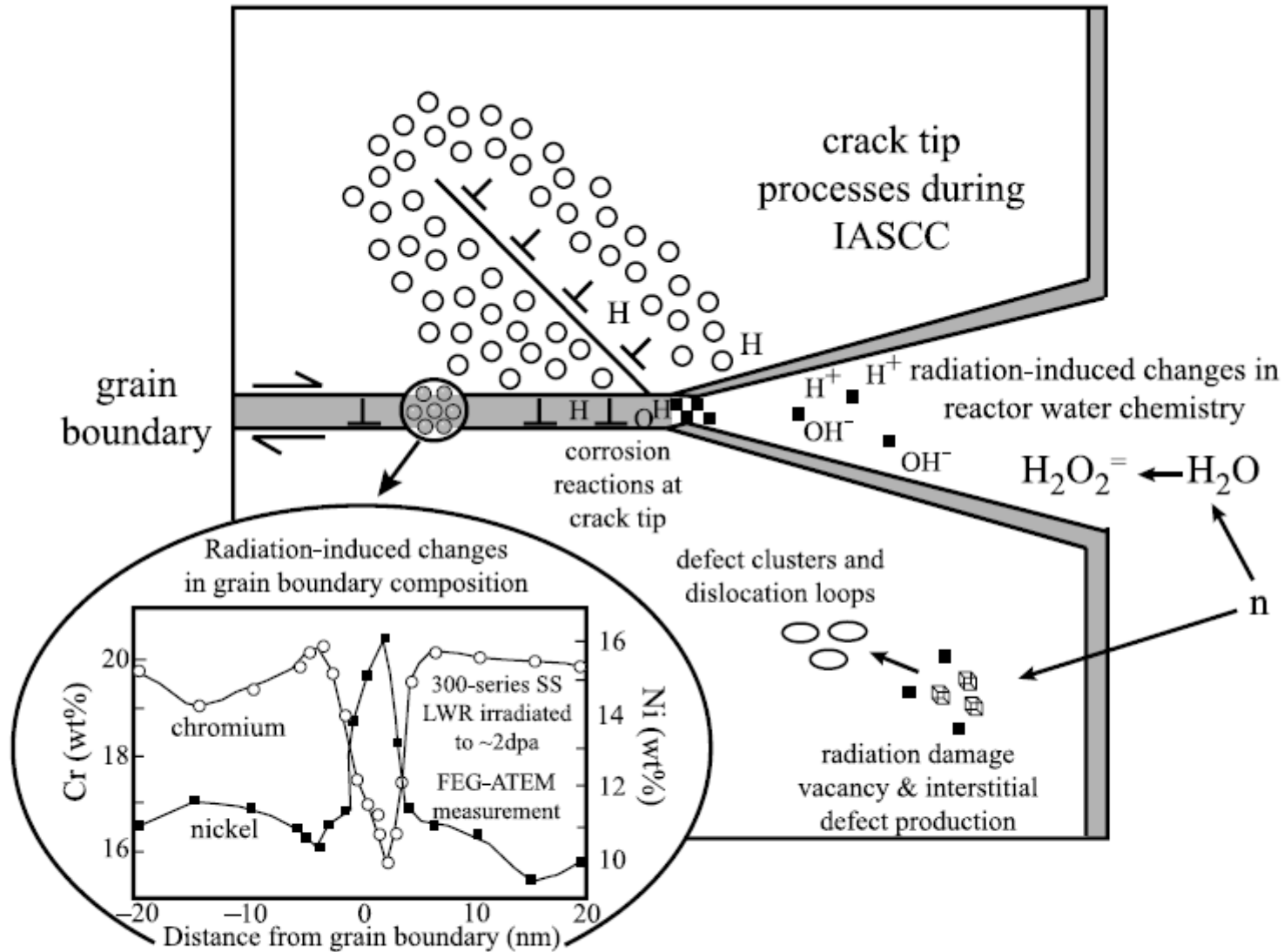


Fig. 15.3. Schematic illustration of mechanistic issues believed to influence crack advance during IASCC of austenitic stainless steels in LWRs (from [6])

EVOLUTION DE LA MICROSTRUCTURE DES METAUX ET ALLIAGES METALLIQUES SOUS IRRADIATION

