

Severe Plastic Deformation

Laszlo S. Toth

Laboratoire d'Etude des Microstructure et de Mécanique des Matériaux
Université de Metz, France

Laboratoire d'Excellence Design des Alliages Métalliques pour
Allègement des Structures, DAMAS

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- **For Introduction: Keywords and objectives**
- **Strain modes in SPD**
- **Strain hardening**
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Keywords and objectives

Keywords:

SPD: Severe Plastic Deformation, Hyperdéformation



UFG: Ultra Fine Grain

BNM: Bulk Nanostructured Materials

NanoSPD: Nanostructured Materials by SPD

NanoSPD6: Metz, 2014, June 30-July 4

Objectives:

To apply SPD for reducing the grain size.

Modern SPD techniques: obtain large strains without changing the shape!

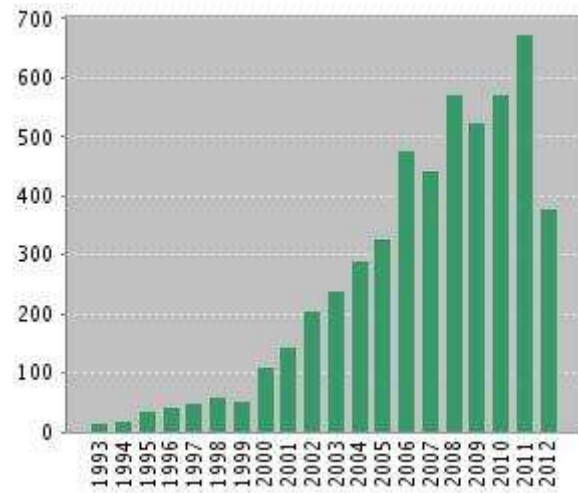
SPD transforms the microstructure, introduces very large amount of new GB.

→ **Grain boundary engineering**

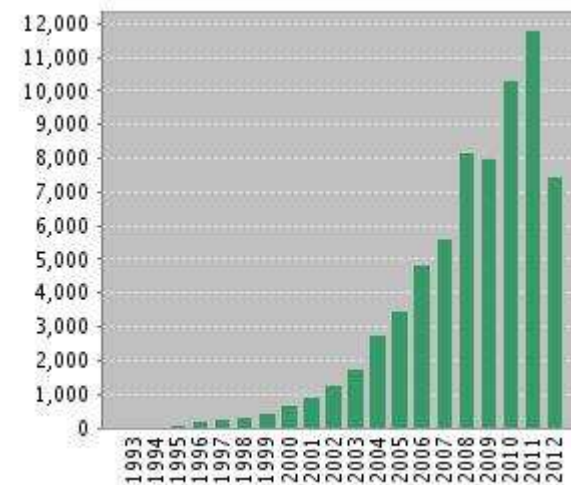
→ **Explore the properties between nano and conventional grain structures, in the UFG regime.**

Publication activity in SPD

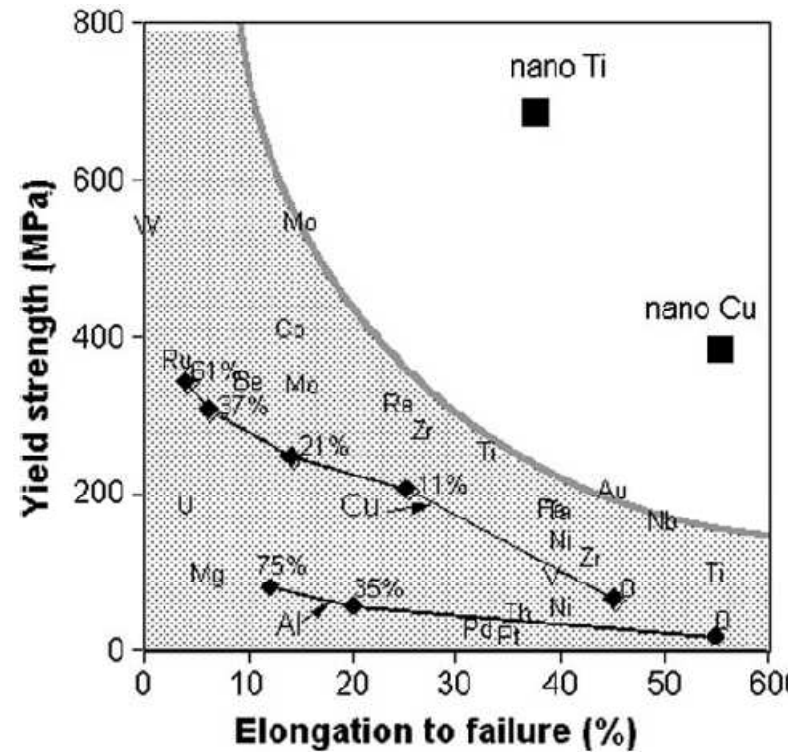
Number of publications



Number of citations

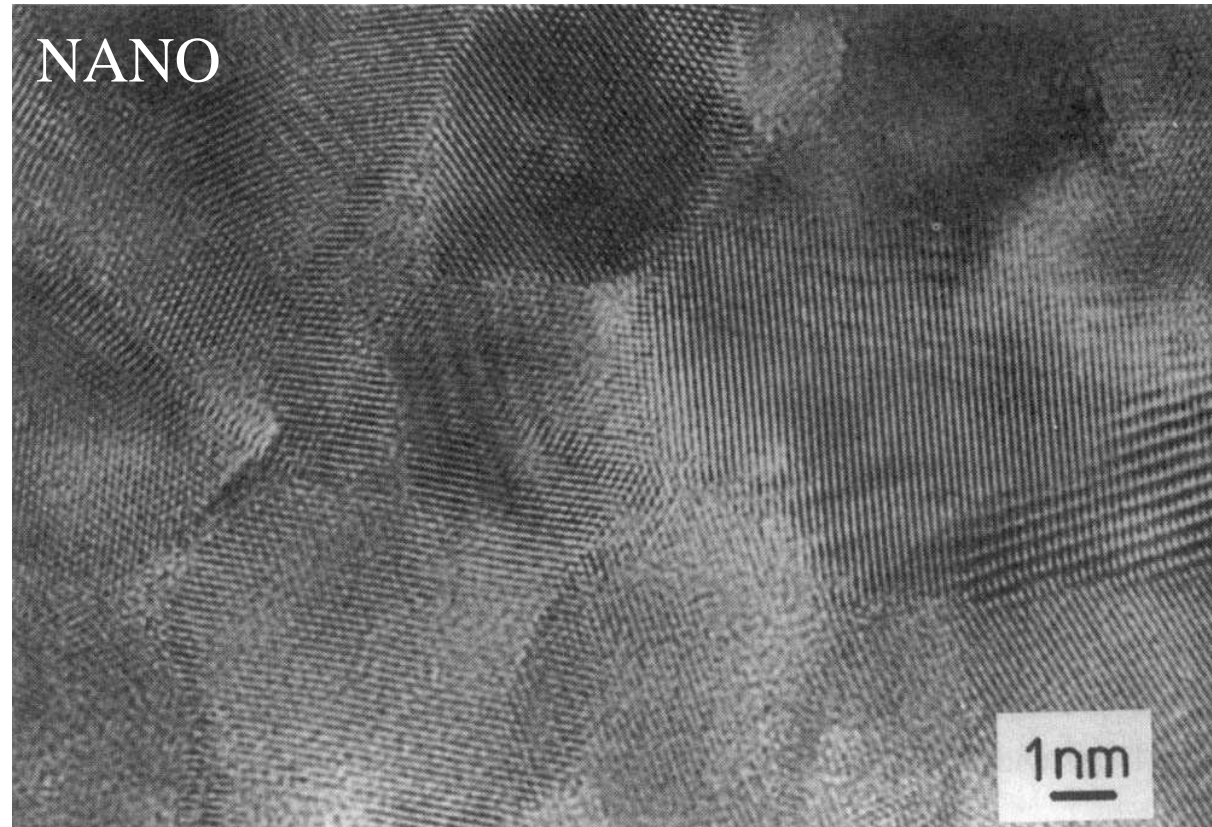


Paradox of strength vs ductility



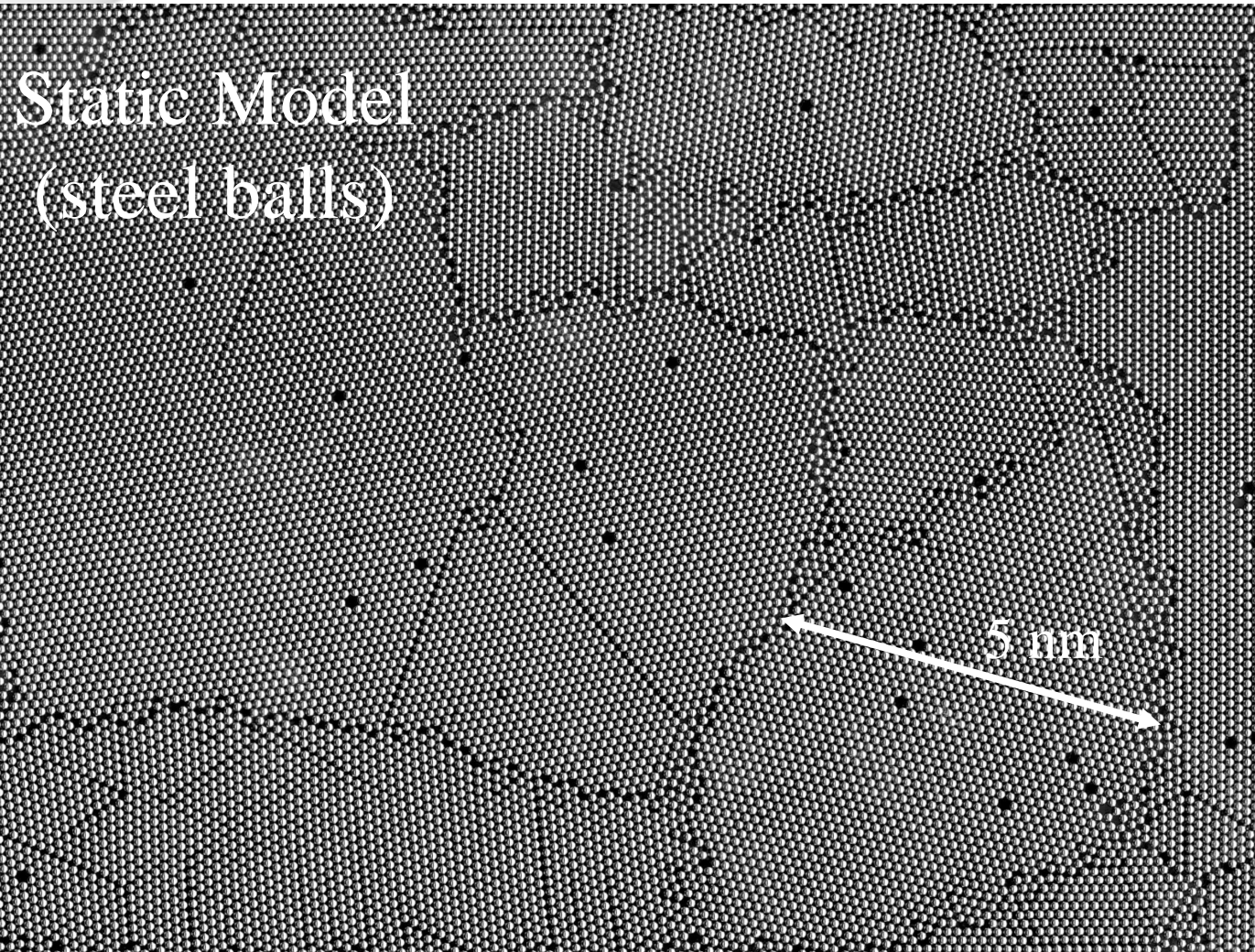
The paradox of strength vs ductility; the nano-Ti and nano-Cu has superior properties

RZ Valiev, IV Alexandrov, TC Lowe, et al., J Mater Res 17 (2002) 5



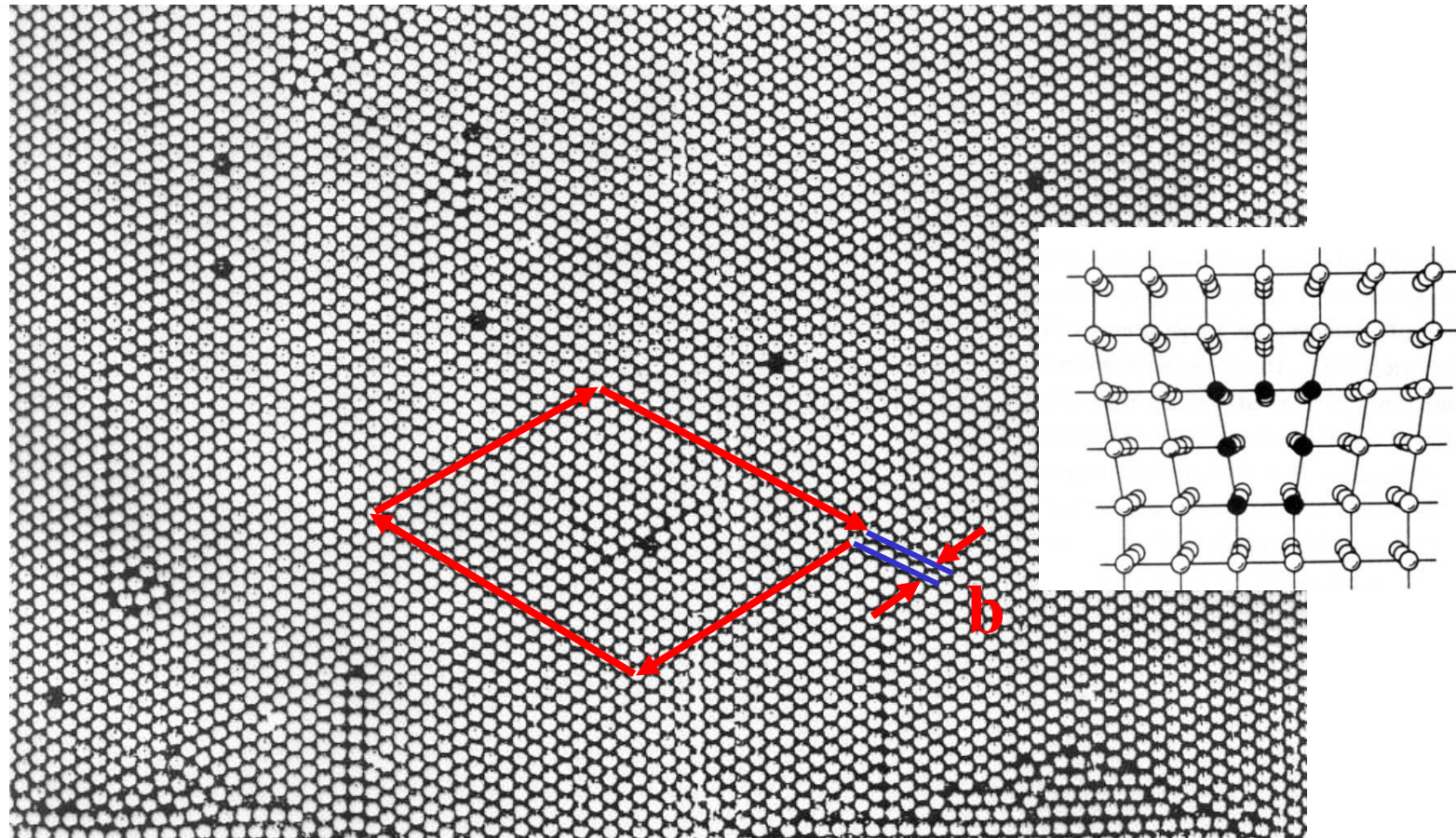
Palladium, HREM

For microstructure teaching



Model for plastic deformation of nanocrystals

For microstructure teaching -dislocation

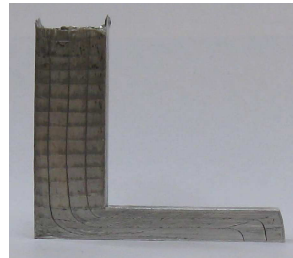


SPD processes

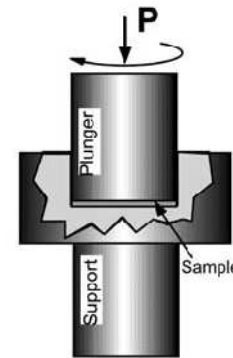
ECAP (ECAE), NECAP, ARB, HPT, HPTT



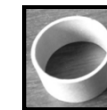
Equal Channel Angular Extrusion



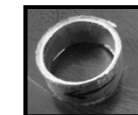
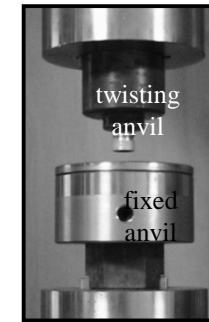
Non-Equal Channel Angular Extrusion



High pressure torsion

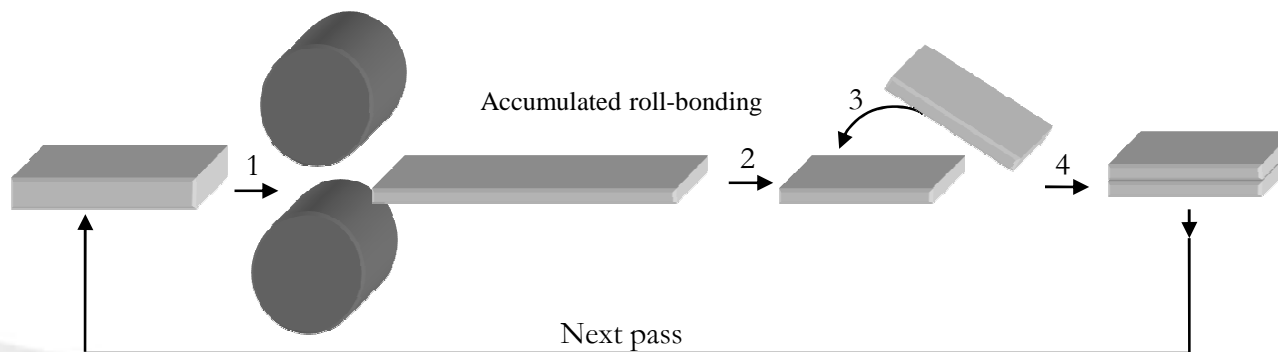


before
HPTT



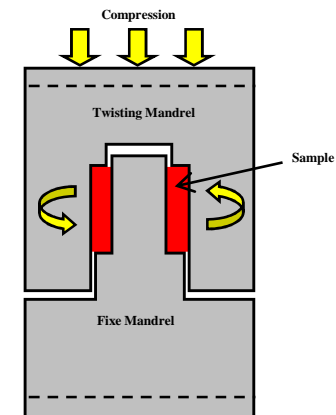
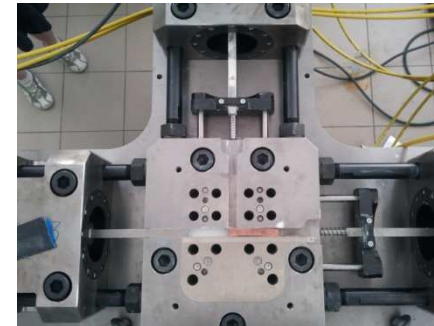
after
HPTT

High Pressure Tube Twisting



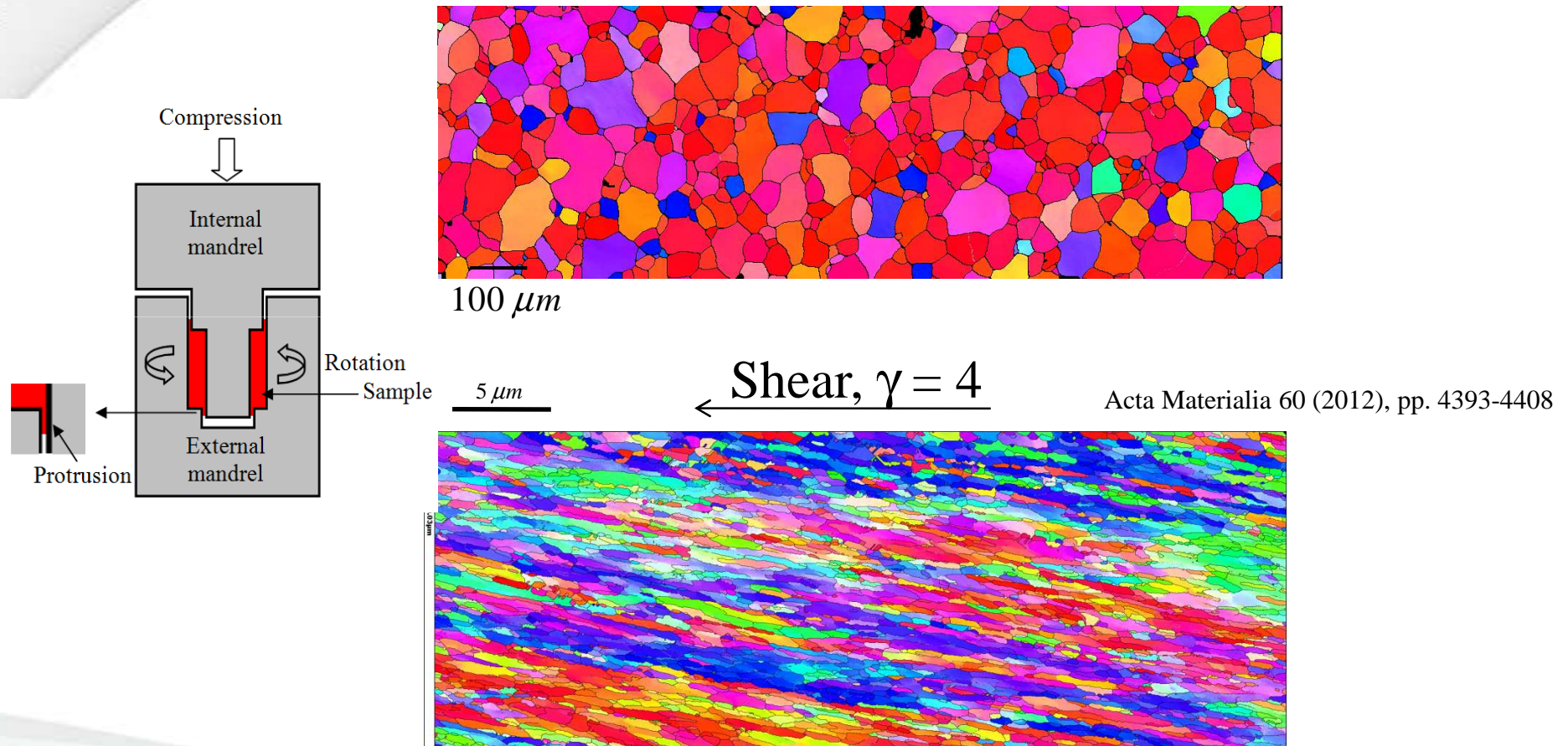
SPD in LEM3, Metz

ECAE



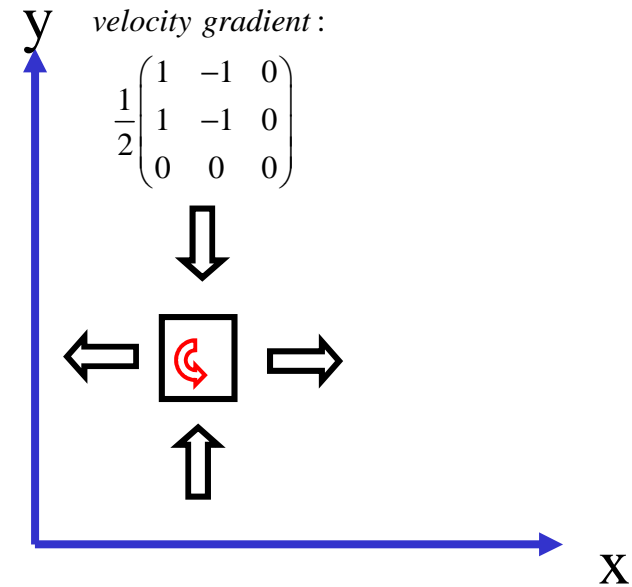
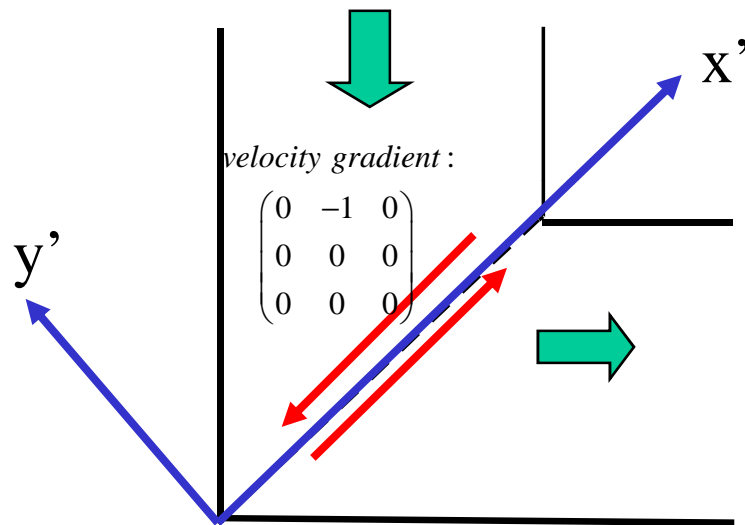
HPTT

Experimental evidence for grain fragmentation in SPD



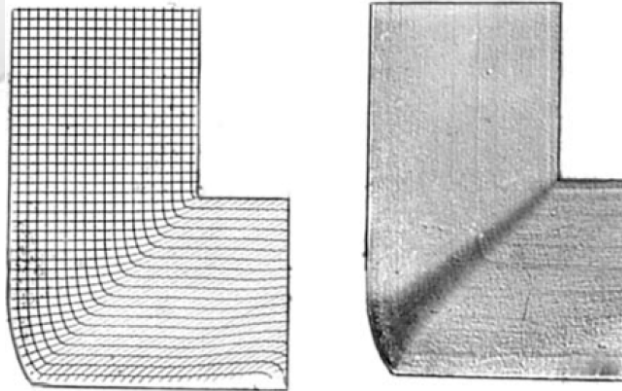
The strain mode in SPD

Strain field in ECAE (simple shear model)

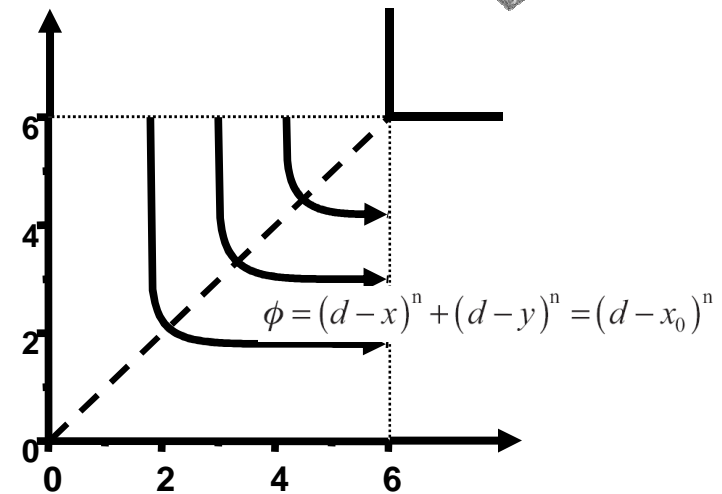


Deformation state:
compression, tension
+ rigid body rotation

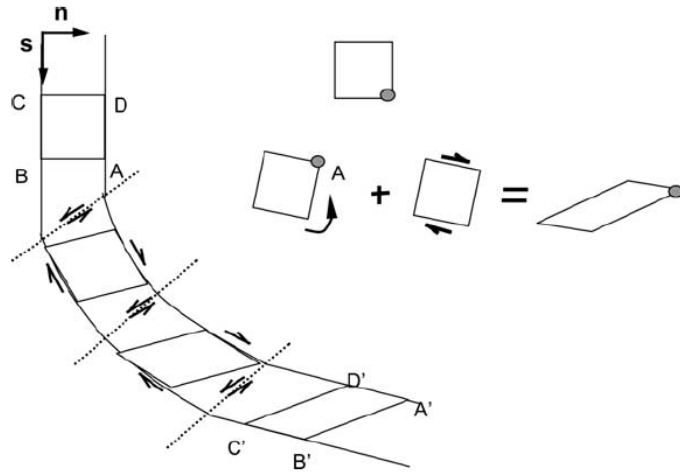
Experiment, Segal, 1999



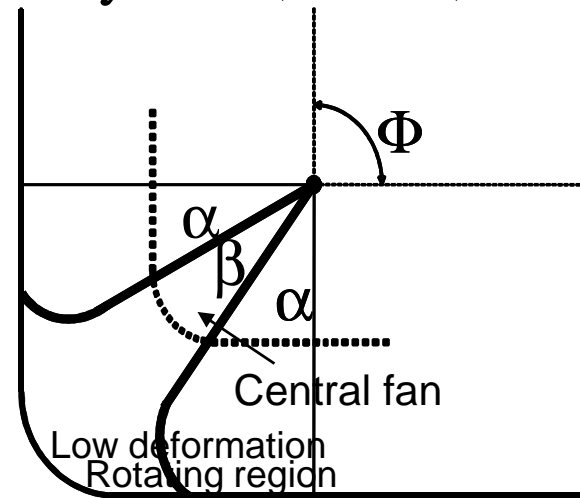
Toth, 2003



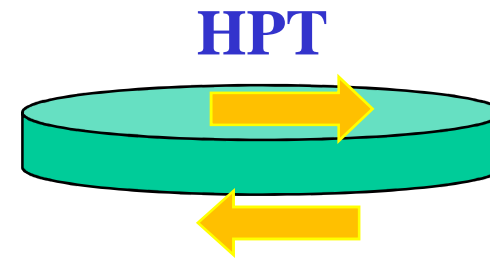
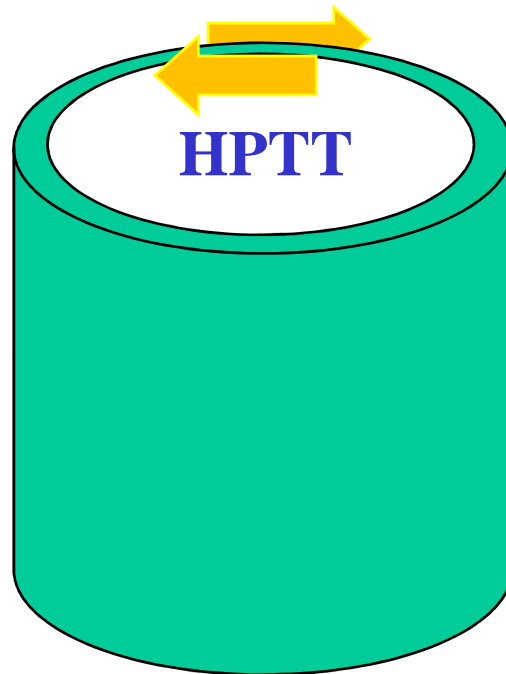
Gholinia, Bate, Prangnell, 2002



Beyerlein, Tome, 2004

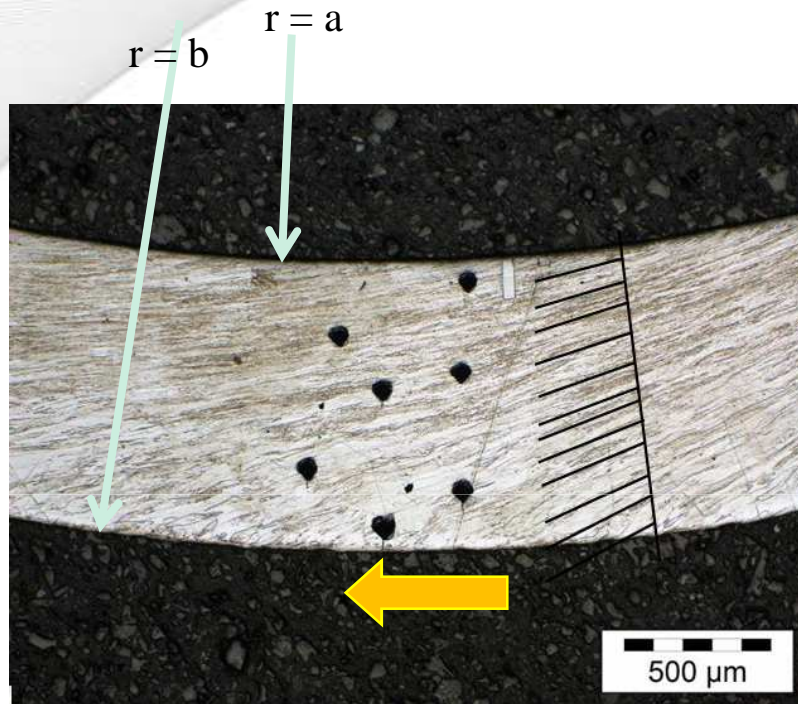


Strain mode in HPTT et HPT

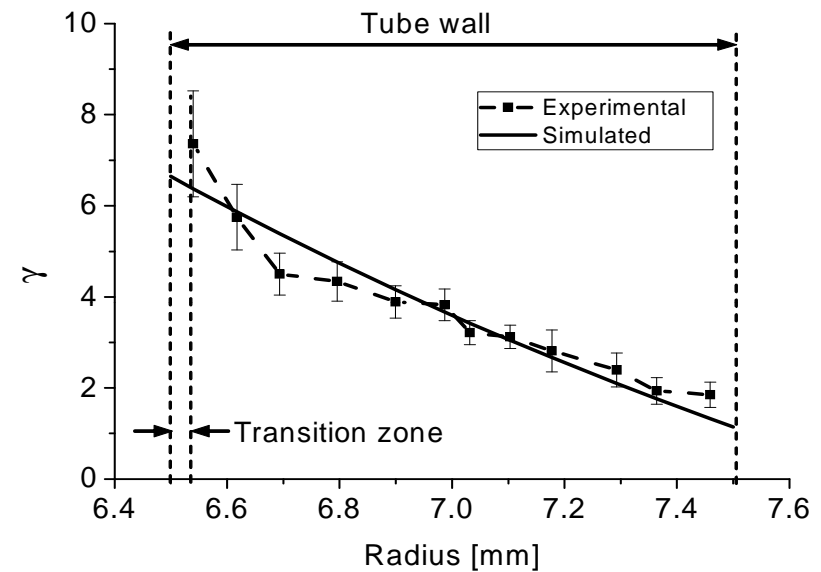


Strain heterogeneity in HPTT

IF steel



Local strain



Average strain:

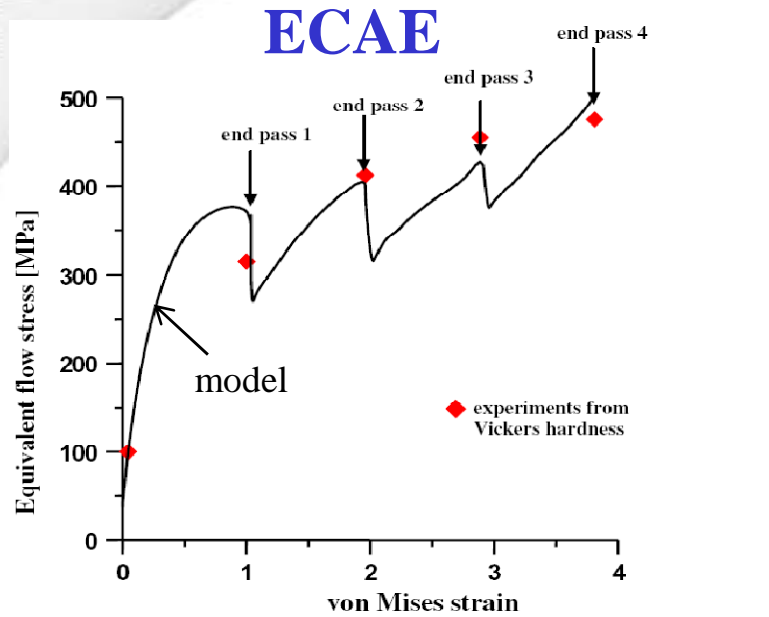
$$\theta = \int_a^b \frac{\gamma(r)}{r} dr \quad \bar{\gamma} = \frac{\theta}{\ln(b/a)}$$

Pougis et al. Scripta Materialia, 66 (2012) 773-776

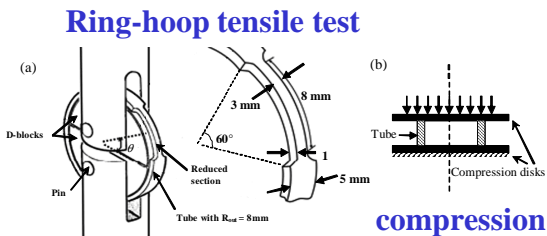
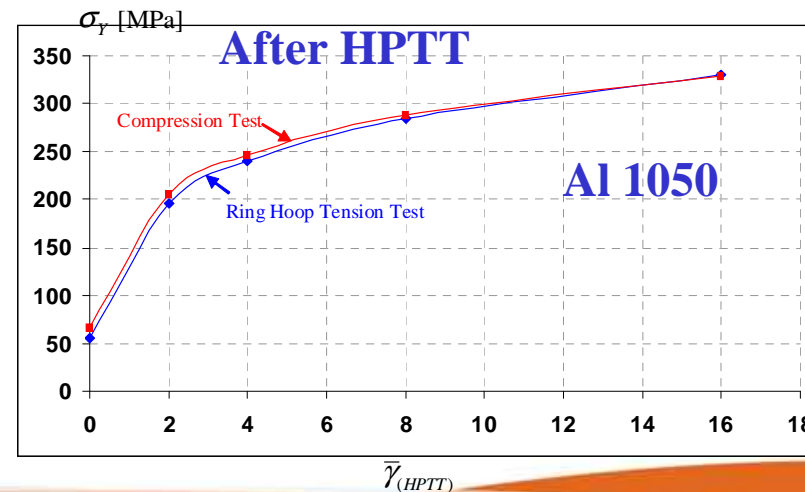
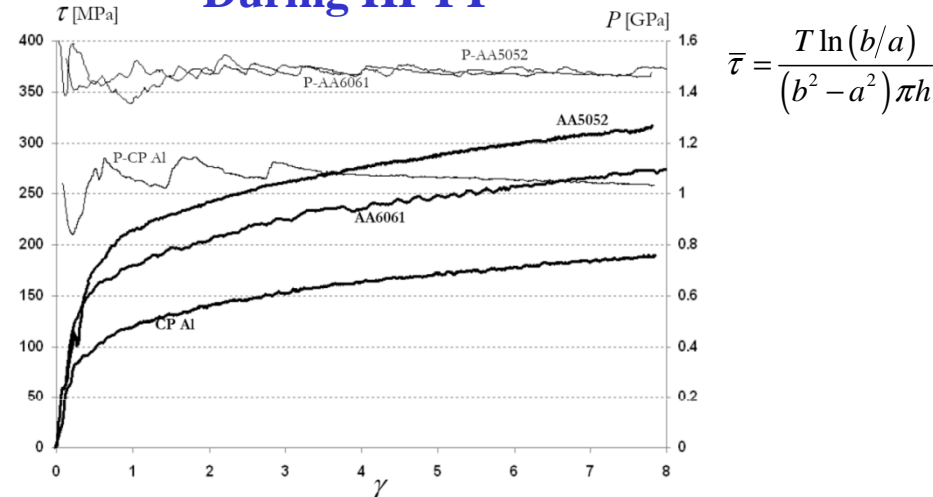
Strain hardening in SPD

Arzaghi et al. Acta Materialia 60 (2012), pp. 4393-4408

L. Toth, Computational Materials Science 32 (2005) 568–576

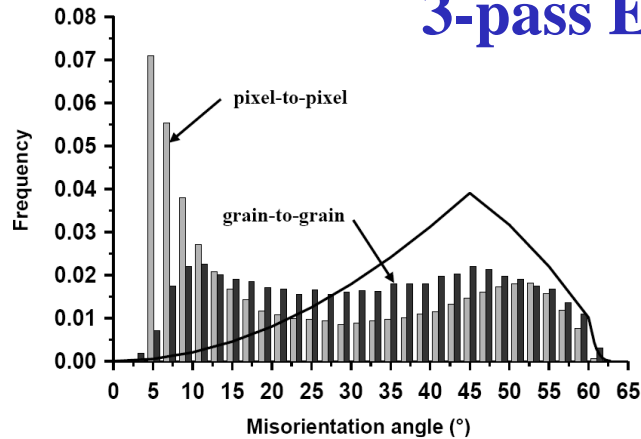


During HPTT

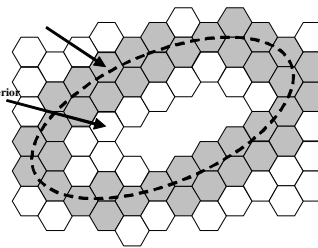
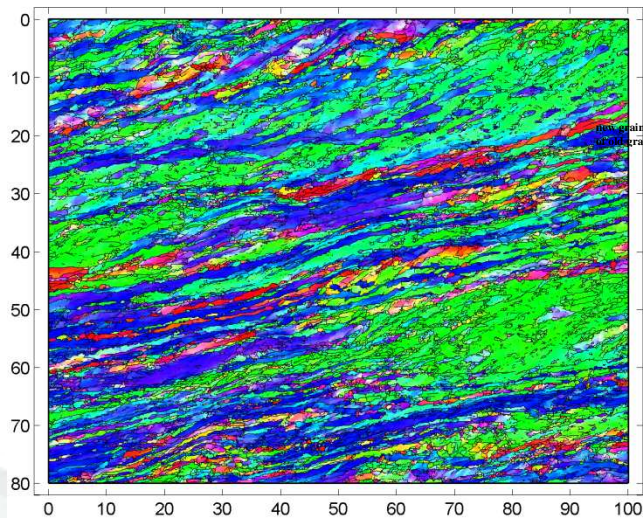
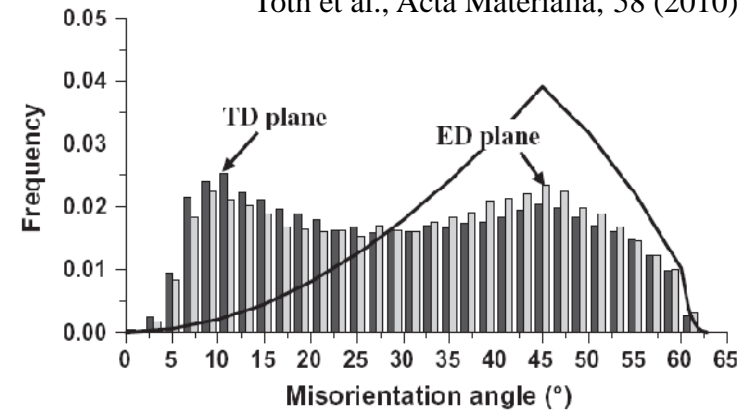


Microstructure features

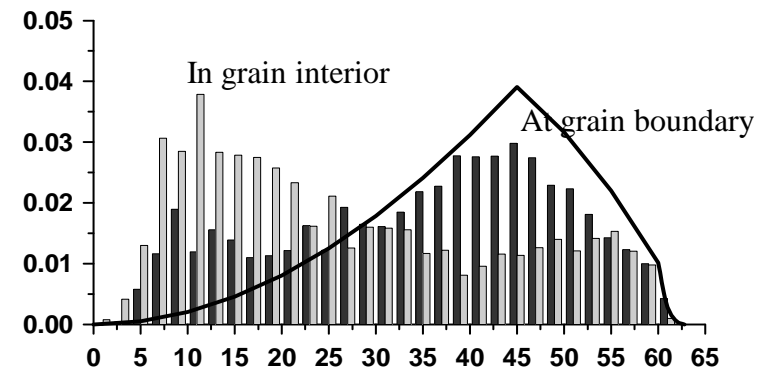
3-pass ECAE Cu



Toth et al., Acta Materialia, 58 (2010) 6706-6716

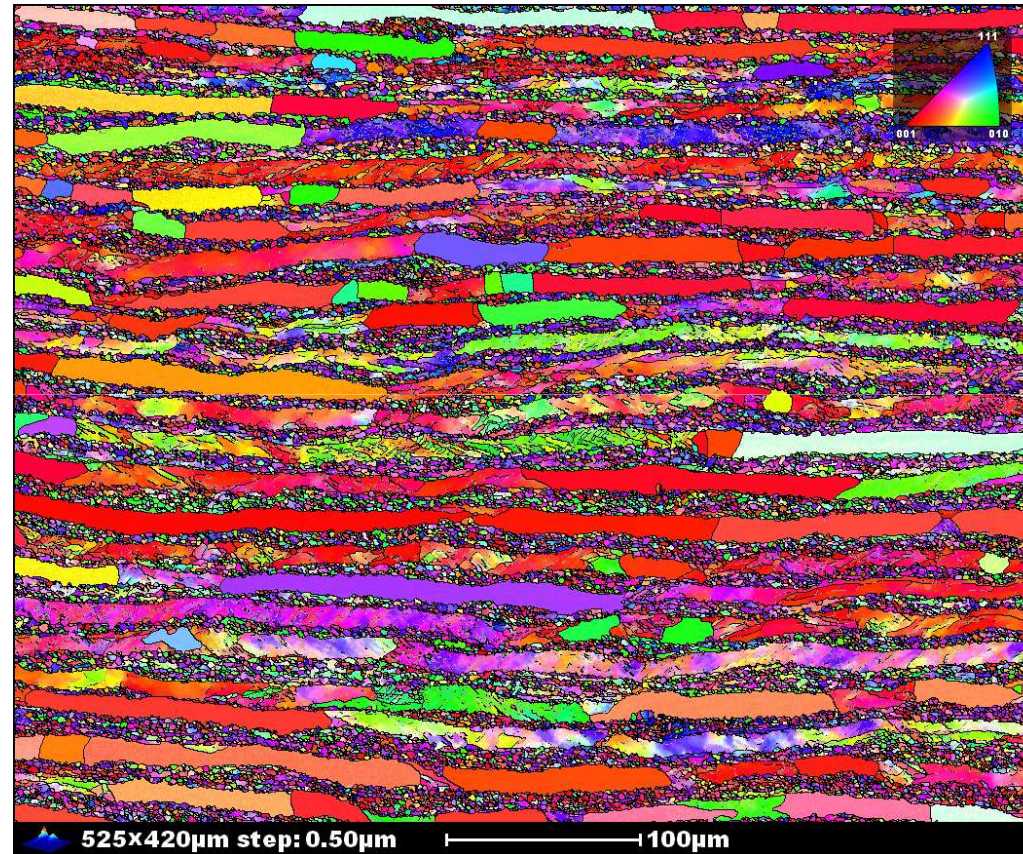


$$v_{total}(\theta) = f_{int} v_{int}(\theta) + f_{OBG} v_{OBG}(\theta)$$



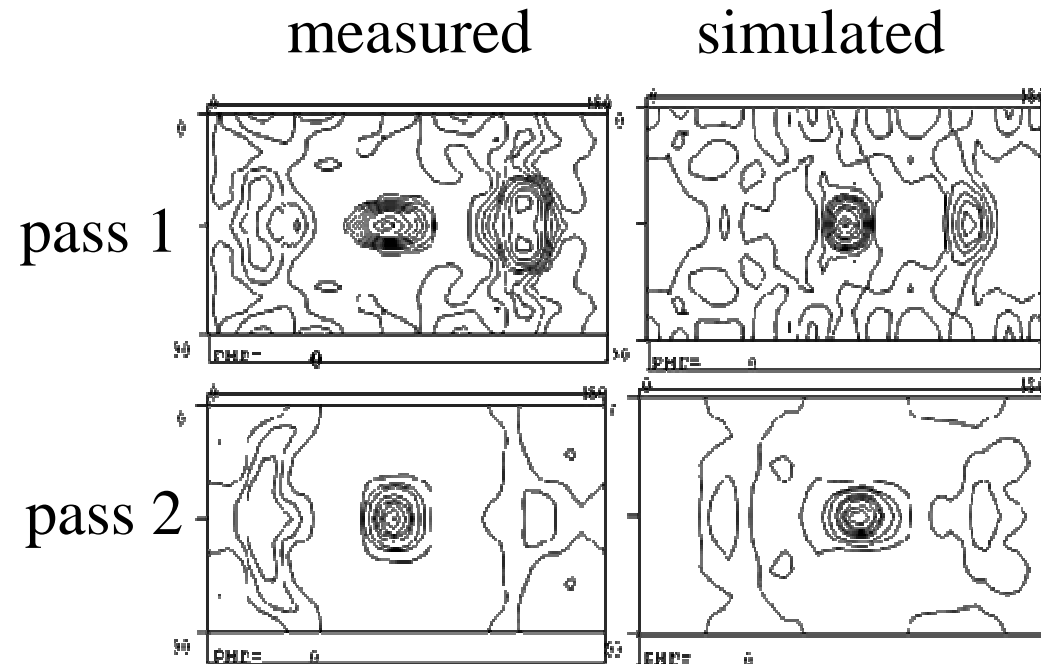
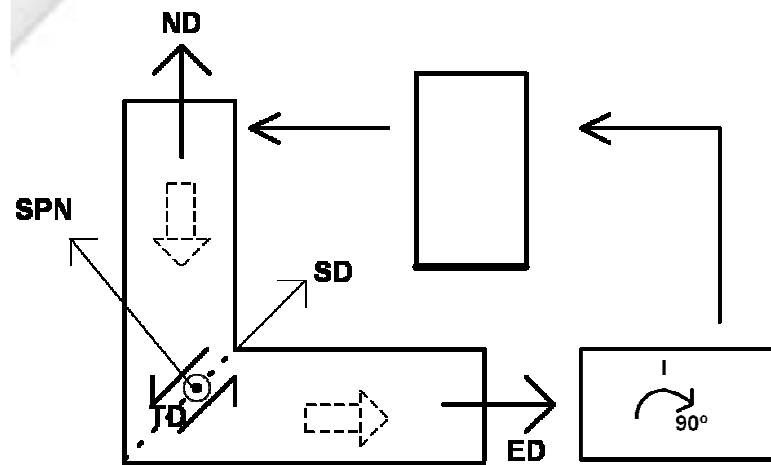
Microstructure in ARB

Al pure +
Al 1050



B. Beausir, T.U. Dresden

Texture evolution



ECAE, Route A, Copper

A new quantitative grain fragmentation model

László S. Toth, Yuri Estrin, Rimma Lapovok, Chengfan Gu
Acta Materialia 58 (2010) 1782-1794

A new model is proposed for grain fragmentation that is based on lattice curvature. The lattice curvature is produced by the grain boundaries where lattice rotation is slowed down.

The new model predicts:

Grain size evolution and distribution

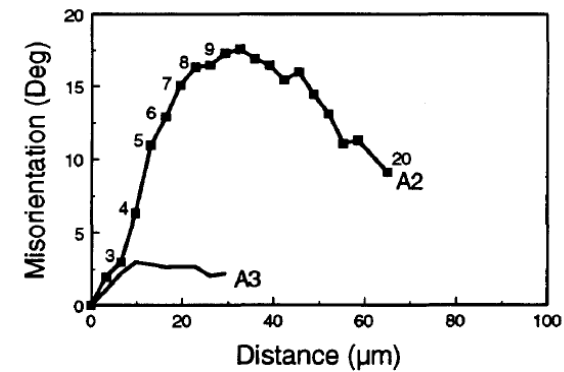
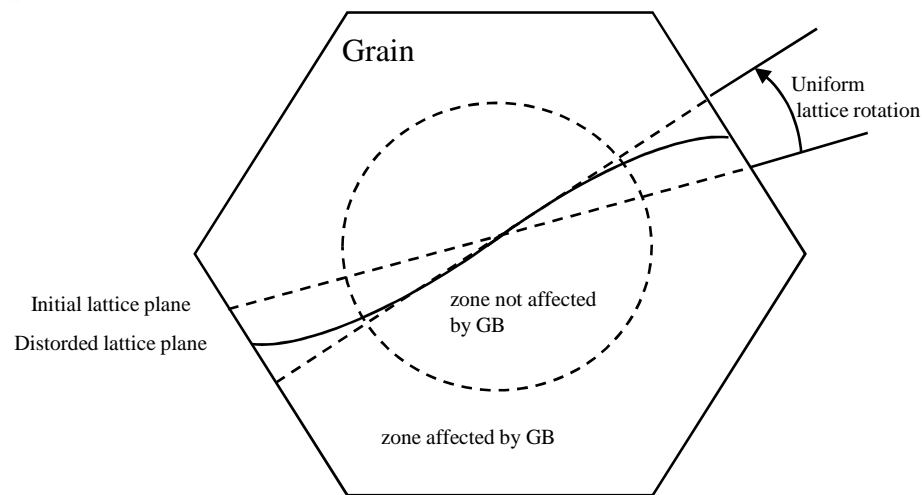
Misorientation distribution of grains

Misorientation of cell walls

Texture development

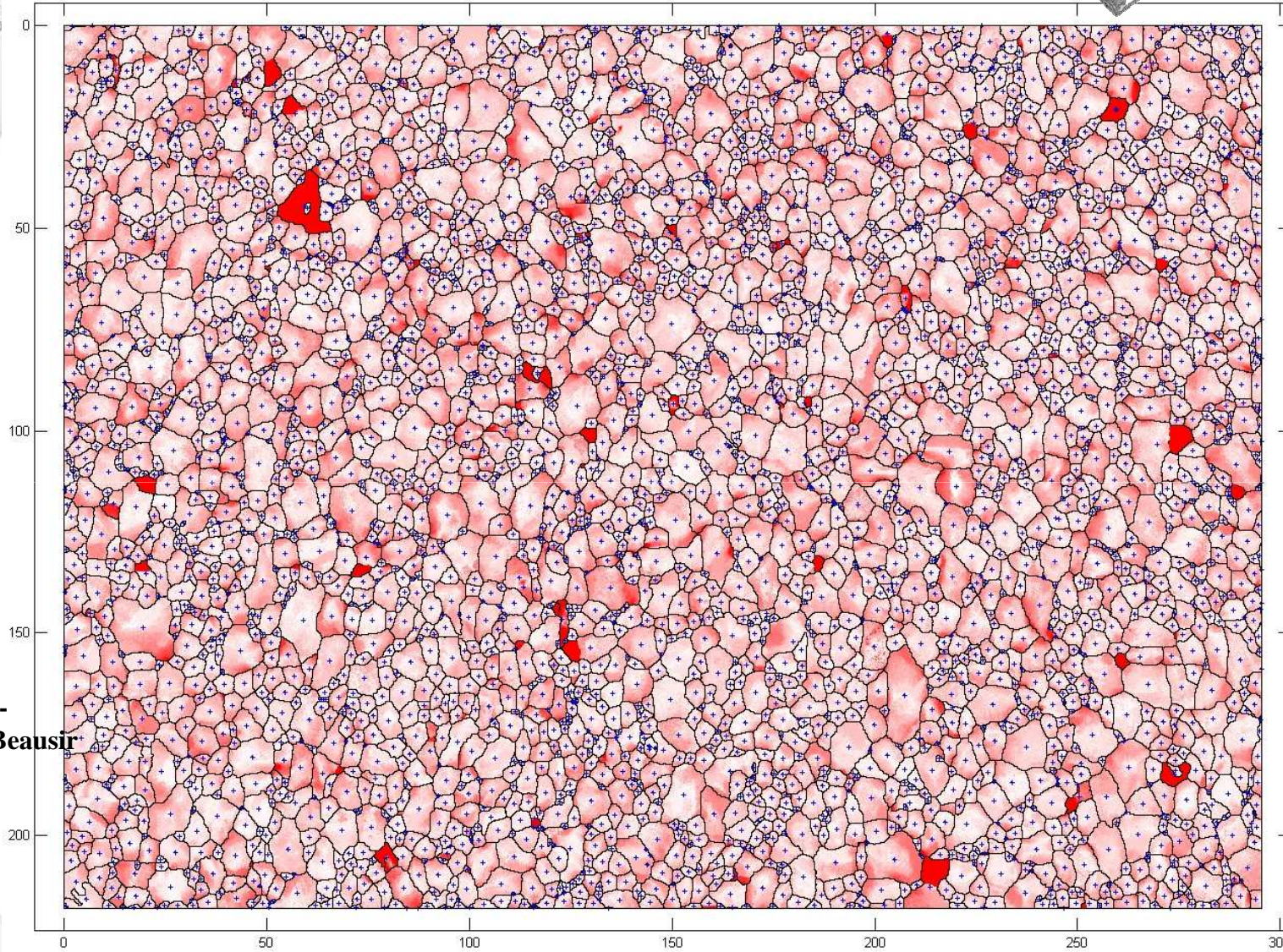
Strain hardening

Lattice curvature in a grain



Al-Si alloy, Skjervold, 1995

Ti rolled to 2% -
Fundenberger-Beausir



C.F. Gu, L.S. Tóth, B. Beausir, *Scripta Materialia*, 2012.

$$\rho_{GND} = \frac{1}{b} \sqrt{\alpha_{ij} \alpha_{ij}}$$

α_{ij} : Nye's dislocation density tensor

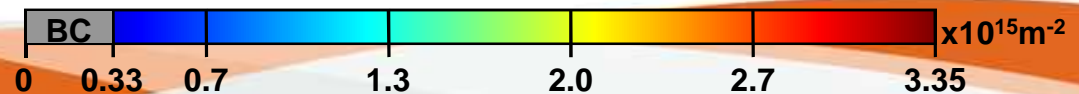
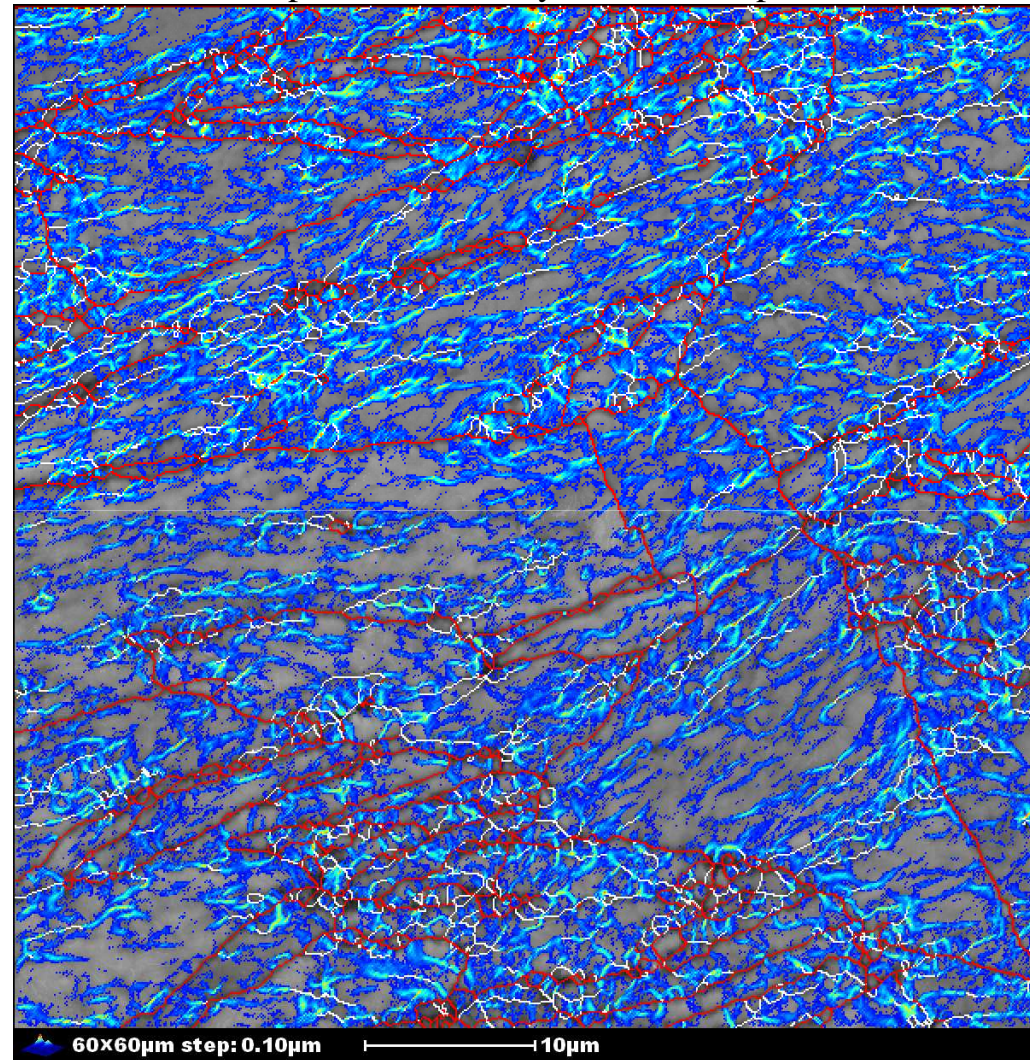
$$\rho_{GND}^{(2D)} = \frac{1}{b} \sqrt{\alpha_{12}^2 + \alpha_{13}^2 + \alpha_{21}^2 + \alpha_{23}^2 + \alpha_{33}^2}$$

Assuming isotropy:

$$\rho_{GND}^{(3D)} = 3\rho_{GND}^{(2D)} / \sqrt{5}$$

$$\rho_{GND}^{(3D)} = 4.38 \times 10^{14} \text{ m}^{-2}$$

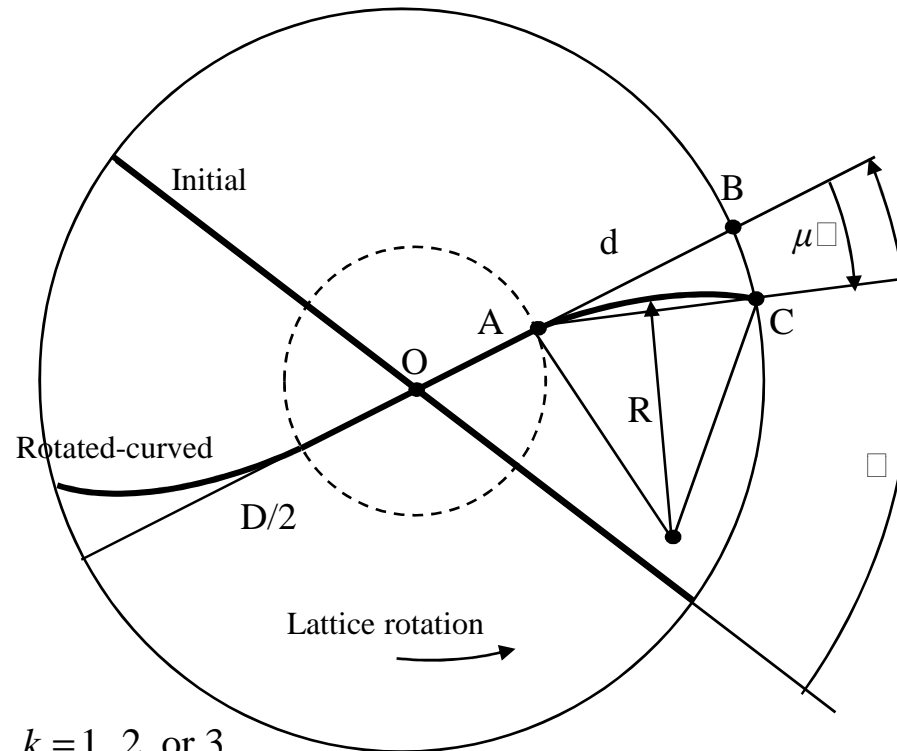
EBSD map of GND density, Cu ECAP 1 pass



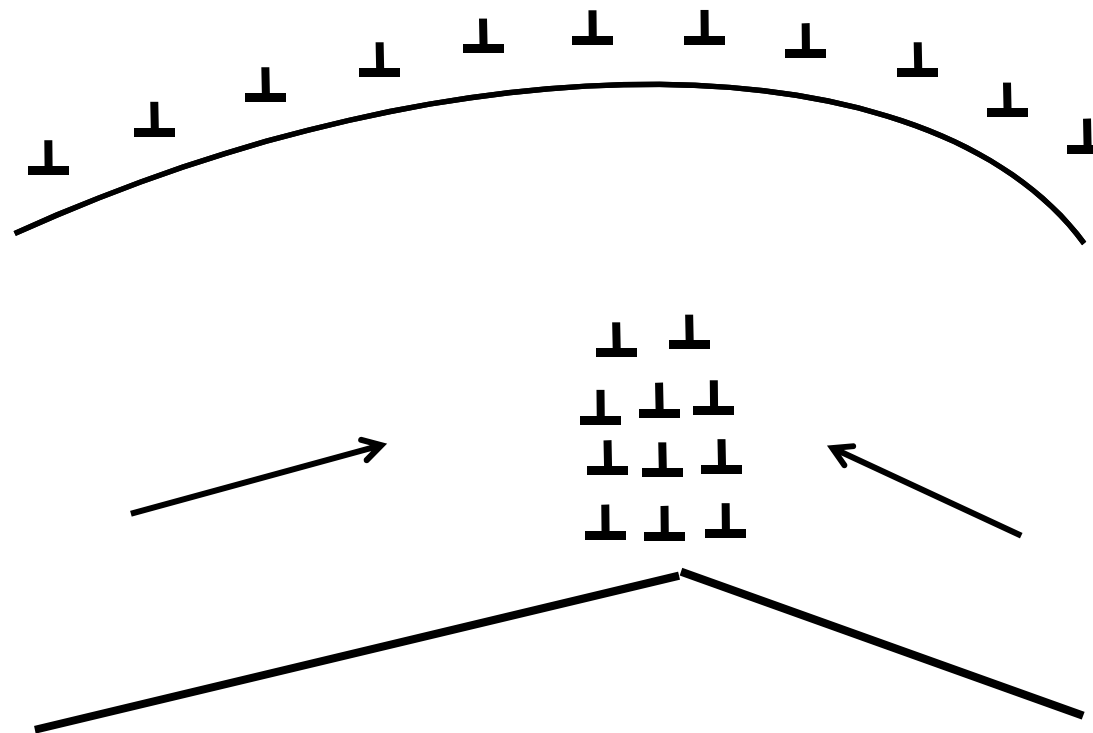
Curvature-induced
dislocation density:

$$\kappa = \frac{1}{R} = \rho_{CID} b$$

$$\rho_{CID} = k \frac{12 \sin(\mu\Omega)}{bD \left[-\cos(\mu\Omega) + \sqrt{\cos^2(\mu\Omega) + 8} \right]}, \quad k = 1, 2, \text{ or } 3.$$

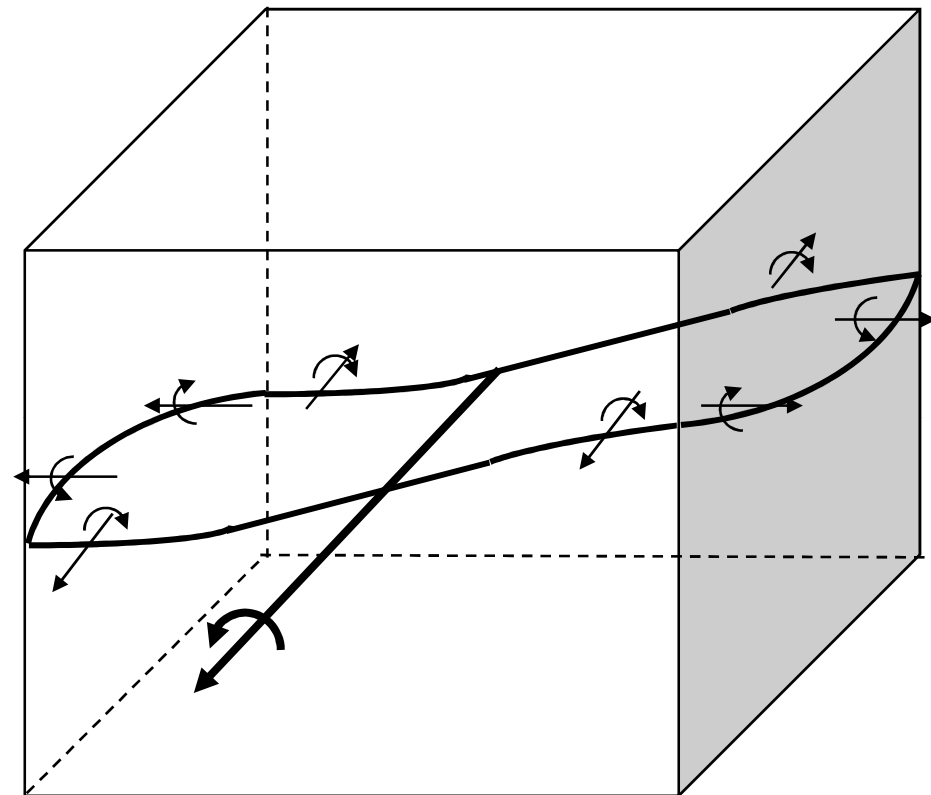
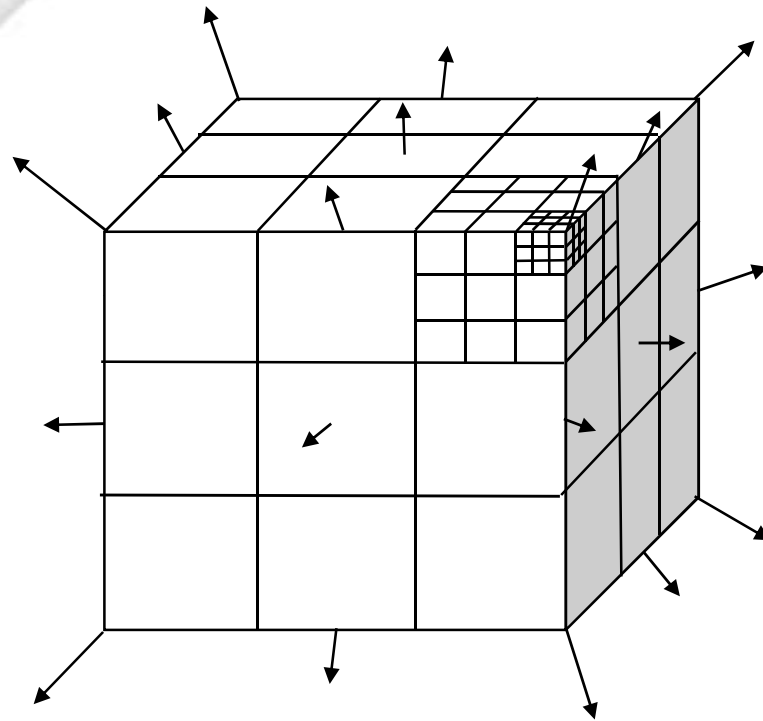


Grain fragmentation procedure



Subgrain rotations:

$$\underline{\dot{\Omega}}_{SG} = \underline{\dot{\Omega}}_G + \underline{\dot{\Omega}}_{SG}^{GB}$$



Application to ECAP of copper

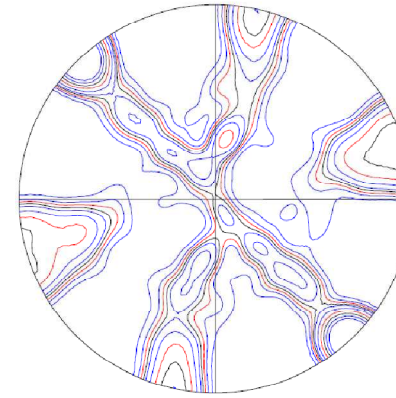
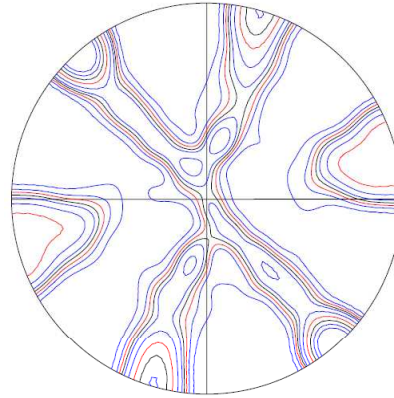
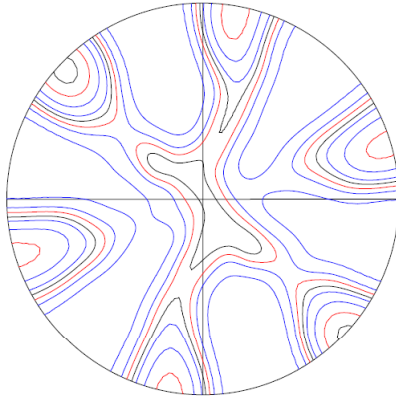
Taylor model, $\mu=0.5$, 500 initial grains \rightarrow 6 million grains

Measured:

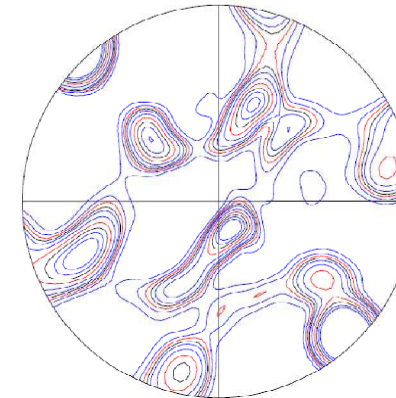
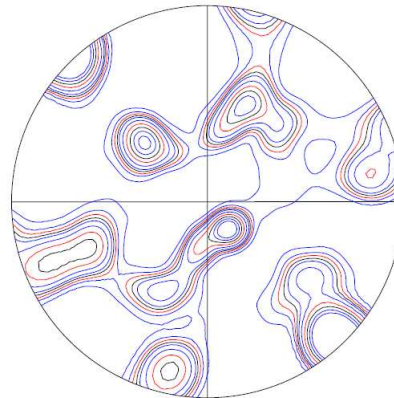
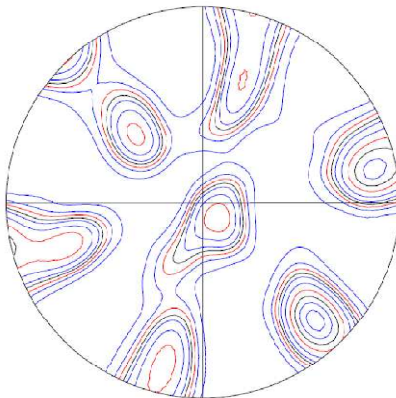
Simulated
with grain
refinement:

Simulated
without grain
refinement:

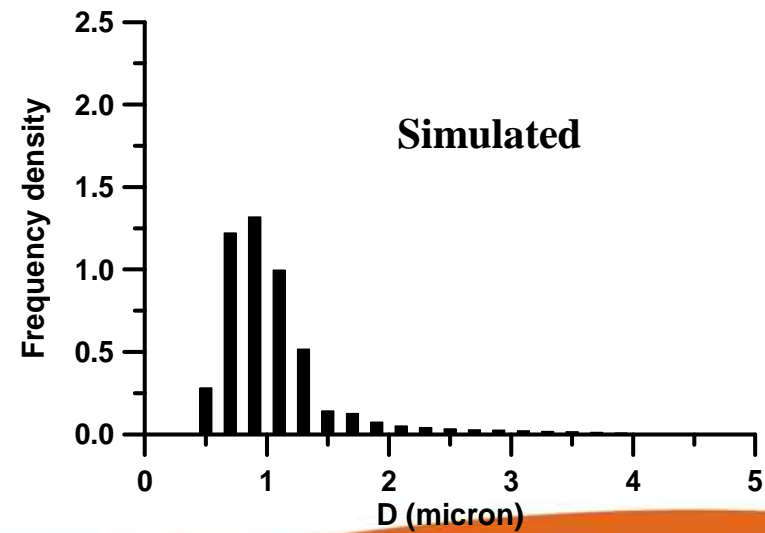
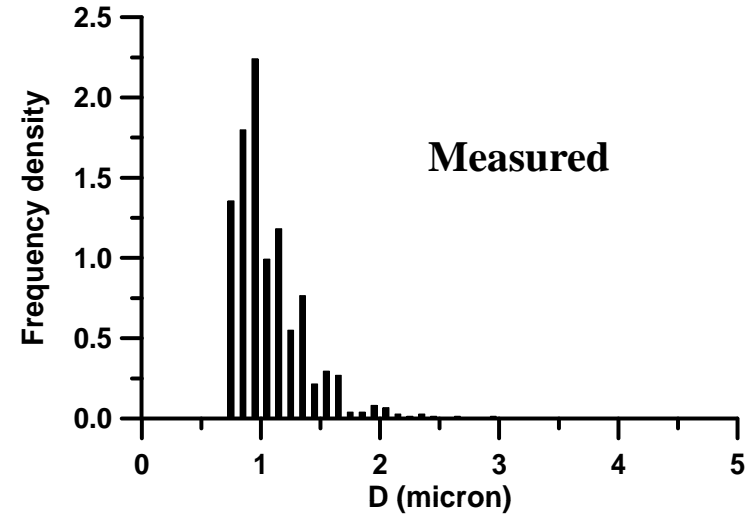
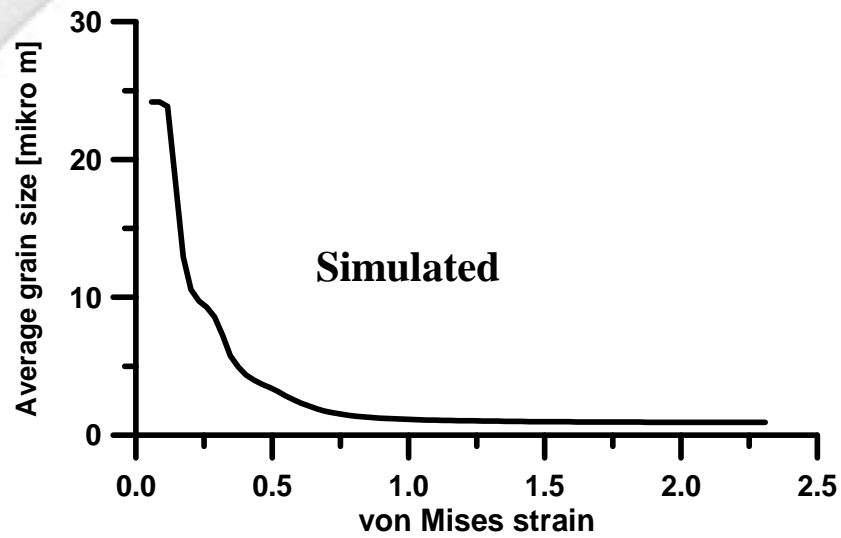
Pass-1



Pass-2, Route Bc



Grain size

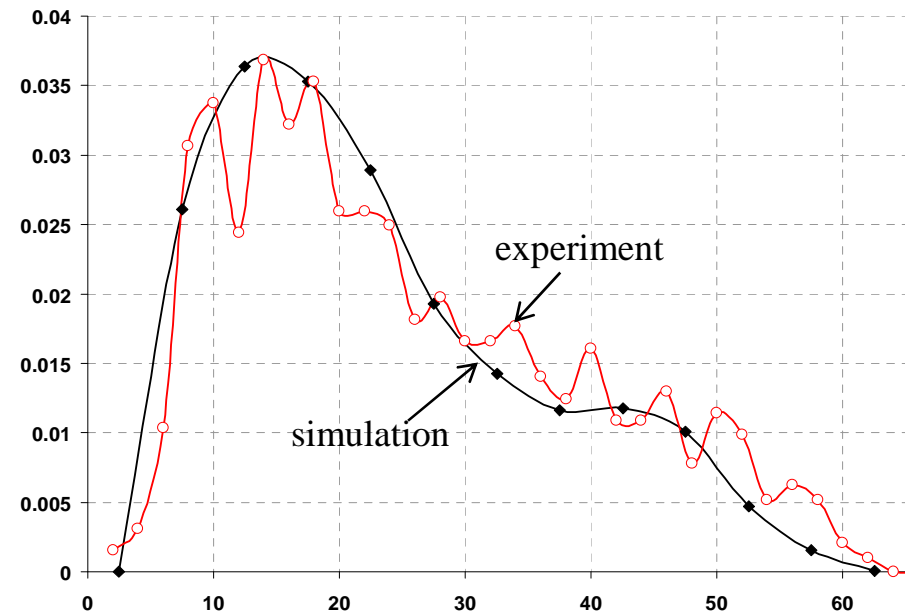
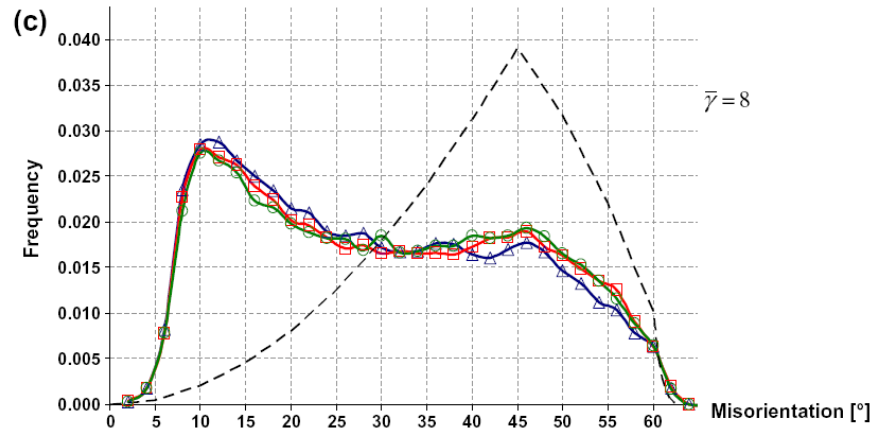
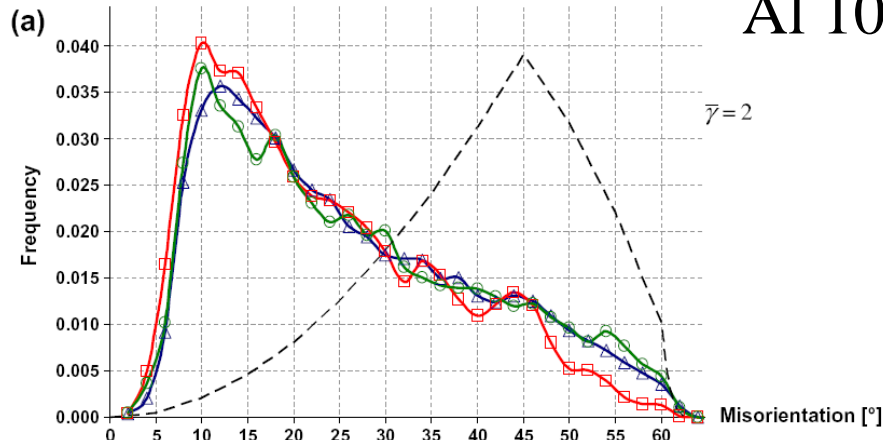


Misorientation distribution (NNMD)

Arzaghi et al. Acta Materialia 60 (2012), pp. 4393-4408

Al 1050 HPTT

M. Arzaghi, Ph.D. thesis, Metz, France, 2010



Next-grain misorientation distribution
Al 1050 HPTT, shear = 4

The dislocation-cell based hardening model

Y. Estrin, L.S. Toth, A. Molinari, Y. Bréchet, *Acta materialia*, 46, 5509-5522, 1998, cited 182 times
L.S. Toth, A. Molinari, Y. Estrin, *J. Eng. Mat. Techn.* 124, 71-77, 2002, cited 70 times.

Cell wall:

$$\dot{\rho}_{ws} = (1 - \xi_1) \frac{6\beta^* \dot{\gamma}_r (1-f)^{2/3}}{bdf} + (1 - \xi_2) \frac{\sqrt{3}\beta^* \dot{\gamma}_r (1-f) \sqrt{\rho_{ws} + \rho_{wg}}}{fb} - k_0 \left(\frac{\dot{\gamma}_w}{\dot{\gamma}_0} \right)^{-1/n} \dot{\gamma}_r \rho_{ws}$$

$$\dot{\rho}_{wg} = \xi_1 \frac{6\beta^* \dot{\gamma}_r (1-f)^{2/3}}{bdf} + \xi_2 \frac{\sqrt{3}\beta^* \dot{\gamma}_r (1-f) \sqrt{\rho_{ws} + \rho_{wg}}}{fb}$$

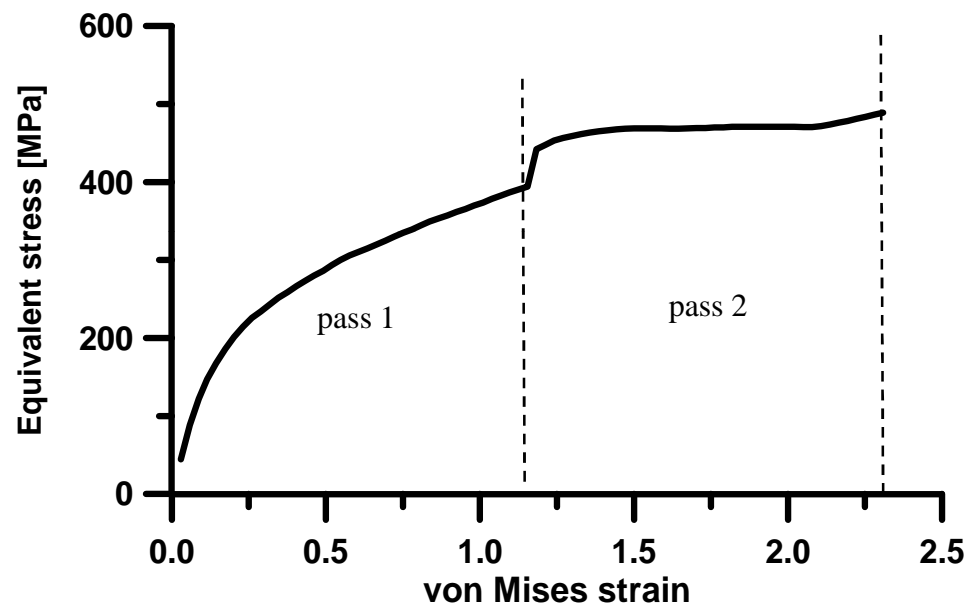
↑ slip from the cells ↑ FR sources for dislocations coming from the cell ↑ annihilation (cross slip)

Cell interior:

$$\dot{\rho}_c = \alpha^* \frac{1}{\sqrt{3}} \frac{\sqrt{\rho_w}}{b} \dot{\gamma}_w - \beta^* \frac{6\dot{\gamma}_c}{bd(1-f)^{1/3}} - k_0 \left(\frac{\dot{\gamma}_c}{\dot{\gamma}_0} \right)^{-1/n} \dot{\gamma}_c \rho_c$$

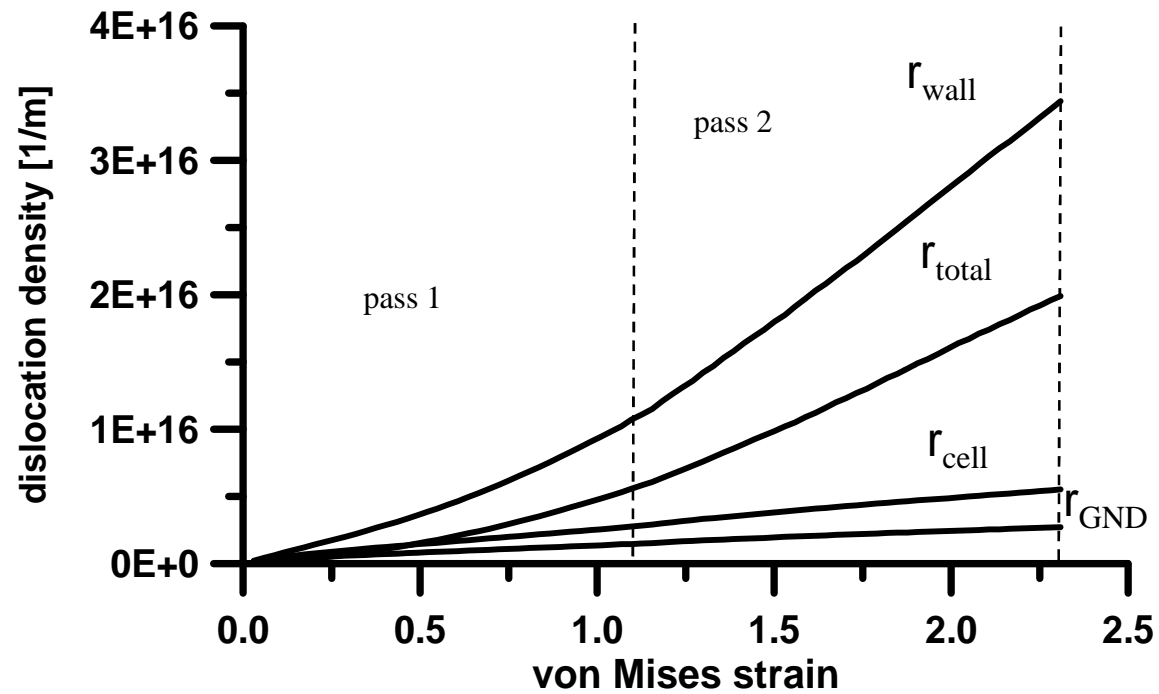
↑ by FR sources from the walls ↑ flux to the walls

Hardening

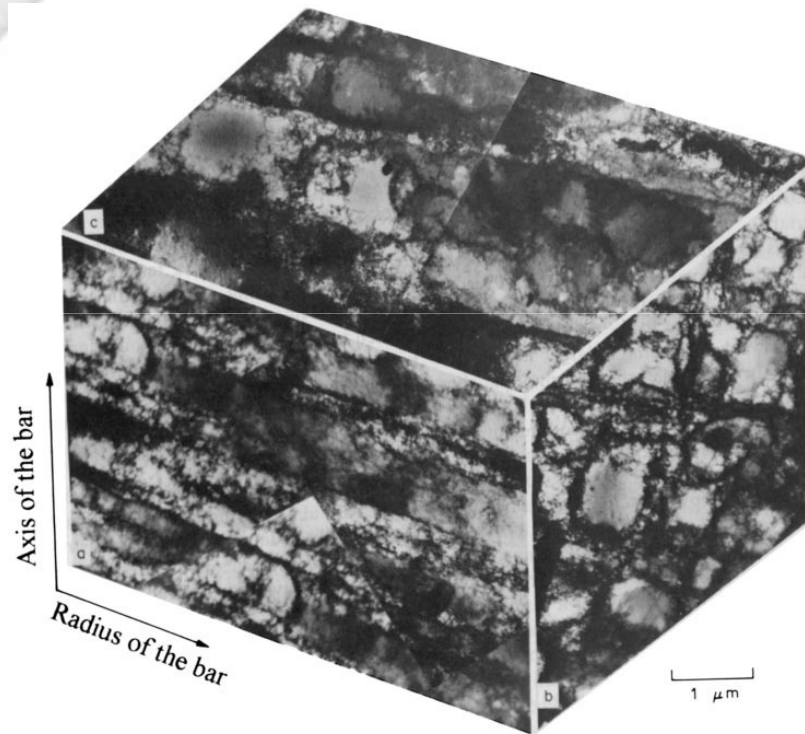


Predicted strain hardening curve

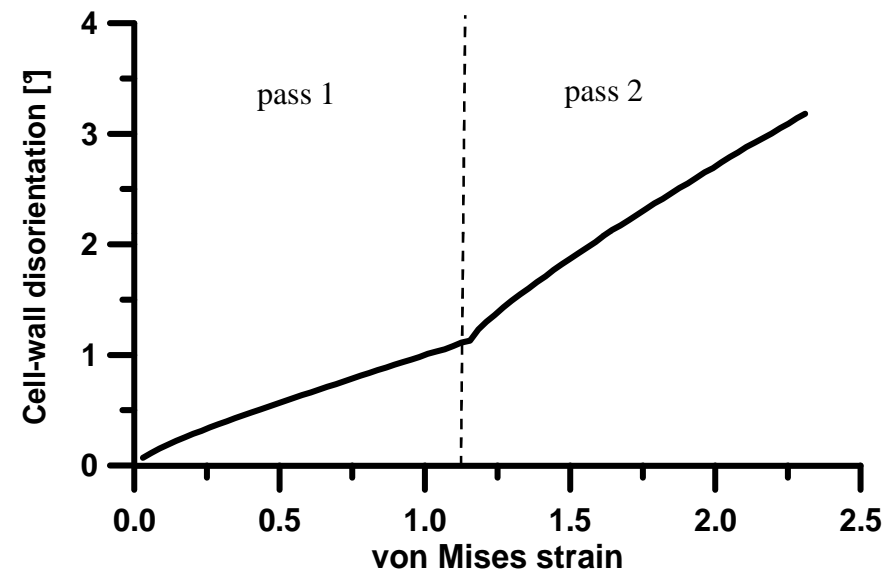
Dislocation densities



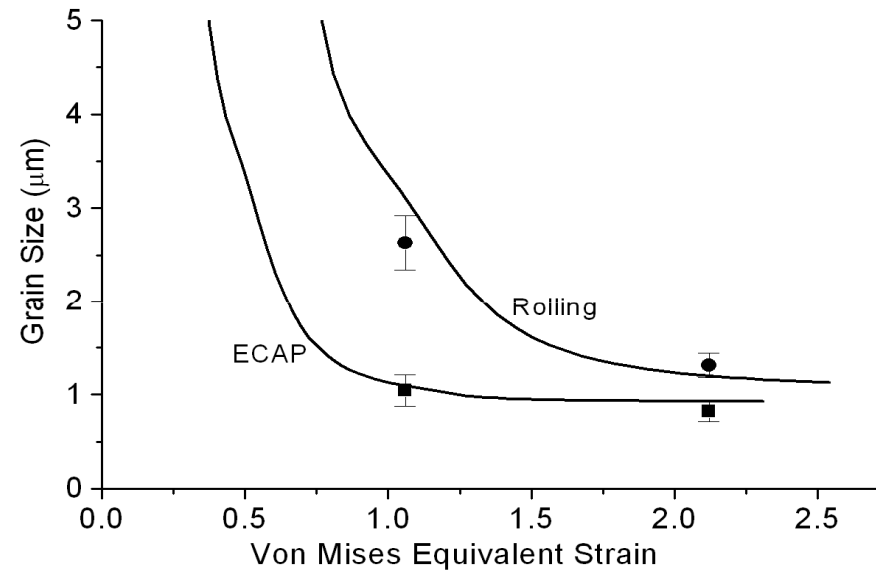
Cell-wall misorientation



$$\theta = bd \rho_{wg}$$



Strain path effect on grain refinement



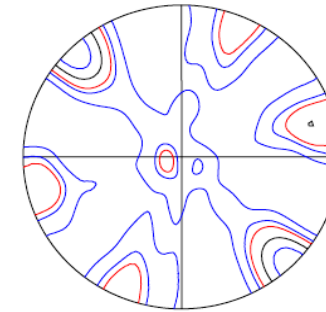
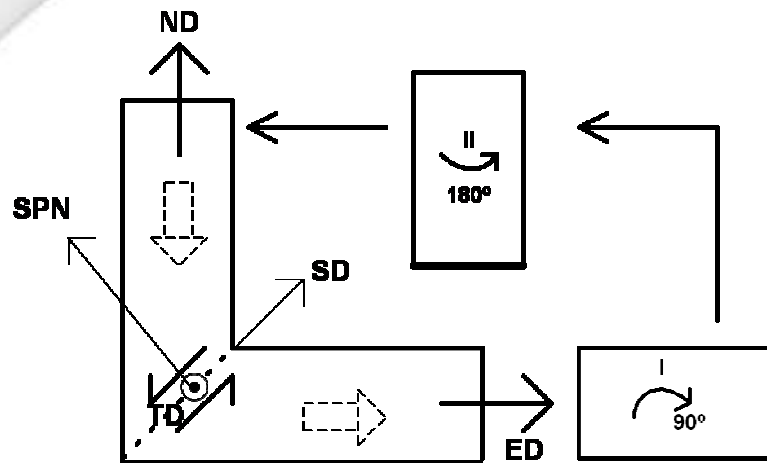
Simulated (continuous lines) and experimental (symbols) development of average grain size obtained in ECAE and rolling

C.F. Gu, L.S. Toth, M. Arzaghi, C.H.J. Davies,
Scripta Materialia, 64 (2011) 284–287

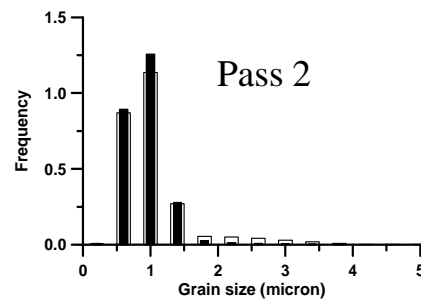
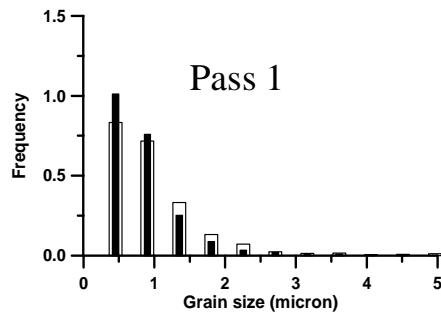
Strain reversal effect on texture and grain refinement

C.F. Gu and L.S. Tóth,
Acta Materialia, 59 (2011) 5749-5757

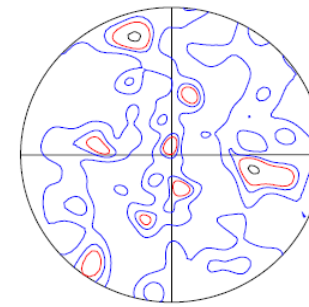
Route C ECAE



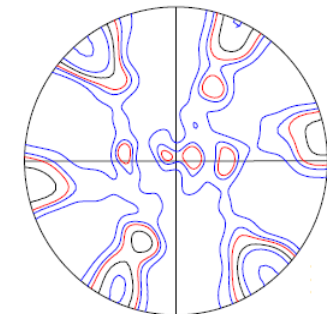
Route C two-pass measured texture



Grain size



Simulated texture by traditional VPSC model



Simulated texture by the new grain refinement model

C.F. Gu, L.S. Toth, C.H.J. Davies,
Scripta Materialia, 65 (2011), 167-170

Strong points and future key issues

Strong points:

- SPD deformation techniques can produce ultra fine grain microstructures with enhanced mechanical properties in bulk form.
- Grain sizes are in the range of sub-micron, in between the minimum grain sizes by DRX et nano-structures, readily feasible
- BNM materials are excellent candidates for biomechanics applications and micro-parts.

Future keys issues:

- Up-scaling from laboratory to industrial processes.
- Mastering of microstructure variations → grand potential in metallurgy
- Understanding the grain subdivision process

Fundamental publications in SPD

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